# TRAFFIC AND PARKING IMPACT ASSESSMENT OF THE PROPOSED CHILD CARE CENTRE AT 5 MARY STREET, NORTHMEAD 



Address: Shop 7, 720 Old Princes Highway Sutherland NSW 2232 Postal: P.O Box 66 Sutherland NSW 1499

Telephone: +61 295217199
Web: www.mclarentraffic.com.au
Email: admin@mclarentraffic.com.au

Division of RAMTRANS Australia ABN: 45067491678 RPEQ: 19457

Transport Planning, Traffic Impact Assessments, Road Safety Audits, Expert Witness

## Development Type: Child Care Centre

Site Address: 5 Mary Street, Northmead

Prepared for: Janssen Designs
Document reference: 220918.01FA

| Status | Issue | Prepared By | Checked By | Approved By | Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Draft | A | KL / MF | LS |  | 1 August 2023 |
| Final | A | MF | LS |  | 10 August 2023 |

Please be aware that all information and material contained in this report is the property of McLaren Traffic Engineering. The information contained in this document is confidential and intended solely for the use of the client for the purpose for which it has been prepared and no representation is made or if to be implied as being made to any third party. Any third party wishing to distribute this document in whole or in part for personal or commercial use must obtain written confirmation from McLaren Traffic Engineering prior to doing so. Failure to obtain written permission may constitute an infringement of copyright and may be liable for legal action.

## TABLE OF CONTENTS

1 INTRODUCTION ..... 1
1.1 Description and Scale of Development ..... 1
1.2 State Environmental Planning Policy (Transport and Infrastructure) 2021 ..... 1
1.3 Site Description ..... 1
1.4 Site Context ..... 2
2 EXISTING TRAFFIC AND PARKING CONDITIONS ..... 3
2.1 Road Hierarchy .....  3
2.1.1 Mary Street ..... 3
2.1.2 Windsor Road ..... 3
2.1.3 Windermere Avenue ..... 3
2.1.4 Margaret Street ..... 3
2.2 Existing Traffic Management ..... 4
2.3 Existing Traffic Environment ..... 5
2.3.1 Existing Road Performance ..... 5
2.4 Public Transport. ..... 8
2.5 Future Road and Infrastructure Upgrades .....  8
3 PARKING ASSESSMENT ..... 9
3.1 Council Parking Requirement ..... 9
3.1.1 Car Parking Demand Analysis ..... 10
3.2 Parking for People with Disabilities ..... 11
3.3 Bicycle \& Motorcycle Parking Requirements ..... 11
3.3.1 The Hills DCP 2012 Bicycle and Motorcycle Requirements ..... 11
3.3.2 Draft Parramatta DCP 2023 Bicycle and Motorcycle Requirements ..... 11
3.4 Servicing \& Loading ..... 13
3.5 Car Park Design \& Compliance ..... 13
4 TRAFFIC ASSESSMENT ..... 14
4.1 Traffic Generation ..... 14
4.2 Traffic Assignment ..... 14
4.3 Traffic Impact ..... 16
5 CONCLUSION ..... 18

## 1 INTRODUCTION

$M^{C}$ Laren Traffic Engineering was commissioned by Janssen Designs to provide a traffic and parking impact assessment of the proposed Child Care Centre at 5 Mary Street, Northmead as depicted in Annexure A.

### 1.1 Description and Scale of Development

The proposed development has the following characteristics relevant to traffic and parking:

- Proposed child care centre accommodating 90 children and 14 staff with the following split:
- 20 children between $0-2$ years old ( 5 staff applied at a rate of 1 per 4 children);
- 20 children between 2-3 years old (4 staff applied at a rate of 1 per 5 children);
- 50 children between 3-6 years old ( 5 staff applied at a rate of 1 per 10 children);
- An at-grade parking area with vehicular access via a proposed two-way driveway from Mary Street, accommodating a total of 24 car parking spaces including:
- 10 visitor car parking spaces including one (1) accessible car parking space;
- 14 staff car parking spaces.


### 1.2 State Environmental Planning Policy (Transport and Infrastructure) 2021

The proposed development does not qualify as a traffic generating development with relevant size and/or capacity under Clause 2.122 of the SEPP (Transport and Infrastructure) 2021. Accordingly, formal referral to Transport for NSW (TfNSW) is unnecessary and the application can be assessed by Parramatta City Council officers accordingly.

### 1.3 Site Description

The subject site is zoned R2 - Low Density Residential under the Parramatta Local Environmental Plan 2023 and is currently occupied by a single dwelling. The site has a single frontage to Mary Street to the south.

The site is generally surrounded by low to medium density residential developments with the Hills School is located approximately 300 m to the east of the site.

### 1.4 Site Context

The location of the site is shown on an aerial photo and a street map in Figure 1 and Figure 2 respectively.


FIGURE 1: SITE CONTEXT - AERIAL PHOTO


FIGURE 2: SITE CONTEXT - STREET MAP

## 2 EXISTING TRAFFIC AND PARKING CONDITIONS

### 2.1 Road Hierarchy

The road network servicing the site has characteristics as described in the following subsections.

### 2.1.1 Mary Street

- Unclassified LOCAL Road;
- Approximately 10 m wide carriageway facilitating one (1) traffic flow lane in each direction and kerbside parking on both sides of the road;
- Signposted $50 \mathrm{~km} / \mathrm{h}$ speed limit;
- $40 \mathrm{~km} / \mathrm{h}$ speed limit applies during school zone hours in front of and to the east of the site's frontage;
- Unrestricted kerbside parking permitted along both sides of the road.


### 2.1.2 Windsor Road

- TfNSW Classified STATE ARTERIAL Road (No. 184);
- Approximately 13 m wide carriageway generally facilitating two (2) traffic flow lanes in each direction;
- An AM / PM contraflow operates south of the signalised intersection of Churchill Drive / Windsor Road whereby one additional lane is provided in the southbound direction during the AM peak hour period, resulting in the loss of one northbound lane during the AM peak period;
- The kerbside lane in the southbound direction is linemarked as "BUS LANE AM" from approximately 120 m south from the intersection of Churchill Drive / Windsor Road.
- Signposted $60 \mathrm{~km} / \mathrm{h}$ speed limit;
- Clearway restrictions apply on both sides of the road at all times.


### 2.1.3 Windermere Avenue

- Unclassified COLLECTOR Road;
- Approximately 10 m wide carriageway facilitating one (1) traffic flow lane in each direction and kerbside parking on both sides of the road;
- Signposted $50 \mathrm{~km} / \mathrm{h}$ speed limit;
- Generally, unrestricted kerbside parking is permitted along both sides of the road.


### 2.1.4 Margaret Street

- Unclassified LOCAL Road;
- Approximately 8 m wide carriageway facilitating two-way traffic flow and kerbside parking on both sides of the road;
- Default $50 \mathrm{~km} / \mathrm{h}$ speed limit;
- Generally unrestricted kerbside parking is permitted along both sides of the road;
- Signposted "No Parking During Sporting Fixtures" restrictions apply along the eastern side of the carriageway.


### 2.2 Existing Traffic Management

- Priority controlled intersection of Mary Street / Margaret Street;
- Priority controlled intersection of Windsor Road / Mary Street;
- Priority controlled intersection of Windsor Road / Windermere Street;
- Signposted restrictions to vehicles exceeding 3 tonnes from accessing Windermere Street from Windsor Road;
- "No Right Turn" restrictions apply at the south Windsor Road approach between the hours of 6AM - 10AM \& 3PM - 7PM Monday to Friday, buses excepted.
- Priority controlled intersection of Anderson Road / Margaret Street;
- Signalised intersection of Windsor Road / Anderson Road;
- Signposted "No Left Turn, Vehicles under 6m Excepted" restriction applies at the south Windsor Road approach;
- Signposted "No Right Turn" restrictions apply at the north Windsor Road approach;
- Signposted "Left Turn on Red Permitted After Stopping" at the NBC Sports Club access driveway approach to the intersection;
- Signposted restrictions to vehicles exceeding 3 tonnes from accessing Anderson Road.


### 2.3 Existing Traffic Environment

Turning movement count traffic surveys were conducted at the intersections of Windsor Road / Mary Street, Mary Street / Margaret Street, William Street / Windermere Avenue, Anderson Road / Margaret Street and Windsor Road / Anderson Road from 7:00am to 9:30am and 2:30pm to 6:00pm on Tuesday 6 June 2023 representing a typical operating weekday. The full survey results are shown in Annexure B for reference.

### 2.3.1 Existing Road Performance

The performance of the surrounding intersections under the existing traffic conditions has been assessed using SIDRA INTERSECTION 9.1. Table 1 summarises the resultant intersection performance data, with full SIDRA results reproduced in Annexure C.

The following considerations have been undertaken to ensure a realistic calibrated model:

- Consideration to the TCS Plan for signalised intersection Windsor Road / Anderson Road (Annexure D);
- A review of the phase length and cycle times based upon video footage which is reproduced in Annexure E for reference:
- Output cycle and phase lengths fall within observed cycle and phase lengths.
- Validation of the model using approach queue lengths for the southern approach of Windsor Road with consideration to the following input modifications:
- Observed average queue lengths along Windsor Road and Anderson Street.

TABLE 1: EXISTING INTERSECTION PERFORMANCES (SIDRA INTERSECTION 9.1)

| Intersection | Peak Hour | Degree of Saturation ${ }^{(1)}$ | Average Delay ${ }^{(2)}$ <br> (sec/veh) | Level of Service ${ }^{(3)(4)}$ | Control Type | Worst Movement |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EXISTING PERFORMANCE |  |  |  |  |  |  |
| Windsor Rd/ Mary St | AM | 1.03 | $\begin{gathered} 1.8 \\ \text { (Worst: >70) } \end{gathered}$ | NA <br> (Worst: F) | Give Way | RT from Windsor Rd |
|  | PM | 1.03 | $\begin{gathered} 0.8 \\ \text { (Worst: >70) } \end{gathered}$ | NA <br> (Worst: F) |  | RT from Windsor Rd |
| Margaret St / Mary St | AM | 0.05 | $3.9$ <br> (Worst: 4.9) | NA <br> (Worst: A) | Give Way | RT from Mary St |
|  | PM | 0.05 | 3.5 <br> (Worst: 4.9) | NA <br> (Worst: A) |  | RT from Mary St |
| Windermere Ave / Mary St / William St | AM | 0.05 | 2.5 <br> (Worst: 5.1) | NA <br> (Worst: A) | Give Way | RT from Mary St / William St |
|  | PM | 0.05 | 2.1 <br> (Worst: 5.3) | NA <br> (Worst: A) |  | RT from Mary St / William St |
| Anderson Rd/ Margaret St | AM | 0.06 | 2.9 <br> (Worst: 5.1) | NA <br> (Worst: A) | Give Way | RT from Margaret St |
|  | PM | 0.05 | $2.7$ <br> (Worst: 5.1) | NA <br> (Worst: A) |  | RT from <br> Anderson Rd |
| Anderson Rd / Windsor Rd | AM | 0.78 | 9.6 | A | Signals | RT from Windsor Rd |
|  | PM | 0.81 | 9.7 | A |  | RT from Anderson Rd |

Notes:
(1) The Degree of Saturation is the ratio of demand to capacity for the most disadvantaged movement.
(2) The average delay is the delay experienced on average by all vehicles. The value in brackets represents the delay to the most disadvantaged movement.
(3) The Level of Service is a qualitative measure of performance describing operational conditions. There are six levels of service, designated from A to $F$, with A representing the best operational condition and level of service $F$ the worst. The LoS of the intersection is shown in bold, and the LoS of the most disadvantaged movement is shown in brackets.
(4) No overall Level of Service is provided for Give Way and Stop controlled intersections as the low delays associated with the dominant movements skew the average delay of the intersection. The Level of Service of the worst approach is an indicator of the operation of the intersection, with a worse Level of Service corresponding to long delays and reduced safety outcomes for that approach.

As shown, most of the relevant intersections are currently performing at a high level of efficiency, with an overall or worst movement Level of Service "A" condition in both the AM \& PM peak hour periods. The Level of Service "A" performance is characterised by low approach delays and spare capacity. However, the intersection of Windsor Road / Mary Street is currently operating with a worst movement Level of Service " F " condition in both the AM \& PM peak hour periods. The worst movement Level of Service "F" performance is indicative of high delays and low to nil capacity remaining.

It should be noted that in some circumstances, with intersections controlled by give way and stop signs, simply examining the highest individual average delay can be misleading. The size of the movement with the highest average delay per vehicle should also be taken into account. Thus, for example, an intersection where all movements are operating at a level of service "A", except one which is at level of service " $F$ ", may not necessarily define the intersection level of service as "F" if that movement is of a relatively small traffic volume. That is, longer delays to a small number of vehicles may not justify upgrading an intersection unless a safety issue were also involved.

The worst movement causing the "F" Level of Service is the right turn movement from Mary Street to Windsor Road northbound. In the AM and PM peak hour periods, the observed peak hour volumes of this movement where nil (0) and one (1) vehicle, respectively. The remaining movements in the intersection operate with a movement Level of Service of "A".

In comparison to the above volumes, the left turn movement from Mary Street had higher volumes of eight (8) and 12 vehicles in the AM and PM peak hour periods, respectively. This suggests that the drivers at the intersection are aware of the high delays required to turn right at this intersection associated with the high two-way flows along Windsor Road and find alternative routes. Indeed, the signalised intersection of Windsor Road / Anderson Road is accessible by vehicles in Mary Street via Margaret Street and Anderson Road, where there are noted to be a high proportion of vehicles turning right from Anderson Road in both the AM and PM peak hour volumes. Accordingly, it is considered likely that drivers from the surrounding residential area travel via this intersection in order to travel northbound along Windsor Road.

Based upon TfNSW crash data from their website, there are no existing cluster of accidents at the intersection of Windsor Road / Mary Street. Therefore, the low right turn volumes from Mary Street at this intersection should not define the operation of the intersection as unacceptable and consideration to intersection upgrades is not required.

### 2.4 Public Transport

The subject site has access to the existing bus stops (ID: 215235 \& ID: 215236) which are located approximately 270 m walking distance northwest and 220 m walking distance to the southwest of the site respectively on Windsor Road. The bus stops collectively service existing bus routes 600 (Hornsby to Parramatta), 601 (Rouse Hill Station to Parramatta via Hills Showground), 603 (Rouse Hill Station to Parramatta via Glenhaven) and 614X (Crestwood to City QVB Express Service) provided by Hillsbus Bus Services.

There are no nearby train stations within an accessible walking distance of the site.
The location of the site subject to the surrounding public transport network is shown in Figure 3.


FIGURE 3: PUBLIC TRANSPORT NETWORK MAP

### 2.5 Future Road and Infrastructure Upgrades

From Parramatta City Council Development Application tracker and website, it appears that there are no future planned road or public transport changes that will affect traffic conditions within the immediate vicinity of the subject site.

## 3 PARKING ASSESSMENT

### 3.1 Council Parking Requirement

Reference is made to The Hills Development Control Plan 2012 Part C Section 1 Parking (hereafter referred to as THDCP 2012) which designates the following parking rates applicable to the proposed development:

### 2.1 General Parking Requirements

Table 1 Required Minimum Car Parking Provisions

| Child Care Centres\# | 1 space per employee plus 1 space per 6 <br> children enrolled for visitors and/or parent <br> parking |
| :---: | :--- |

Also see 2.1.1. (e)
\# Set down areas are to be provided for these land uses - refer to section 2.6.

### 2.1.1. General

(e) Car parking for child care centres must be situated in a convenient location, allowing for safe movement of children to and from the centre.

Table 2 presents the parking requirements of the proposal according to THDCP 2012 parking requirements.

TABLE 2: THDCP 2012 PARKING REQUIREMENTS

| Land Use | Scale | Rate | Spaces Required | Spaces Provided |
| :---: | :---: | :---: | :---: | :---: |
| Child Care <br> Centre | 90 Children | 1 per 6 children | 15 | 10 |
|  | 14 Staff | 1 per staff member | 14 | 14 |
| TOTAL | - | - | $\mathbf{2 9}$ | $\mathbf{2 4}$ |

As shown, strict application of THDCP 2012 results in a required provision of 29 car parking spaces (with 15 for visitor use and 14 for staff use). The proposed plans detail the provision of $\mathbf{2 4}$ car parking spaces (including 10 for visitor use and 14 for staff use), resulting in a numerical shortfall of five (5) visitor spaces from THDCP 2012 requirements.

However, the City of Parramatta Council recently released a draft Parramatta Development Control Plan for public exhibition which is expected to prevail over The Hills DCP when it comes into effect. This DCP will consolidate five DCPs that currently apply across the City of Parramatta LGA, including The Hills DCP 2012. The relevant parking rates provided in the Draft Parramatta Development Control Plan 2023 (DPDCP 2023) are reproduced below for reference:

### 6.2 Parking and Vehicular Access

Table 6.3.1-Minimum car parking rates

## Child care centres 1 space for every 4 children in attendance

Table 3 presents the parking requirements of the proposal according to the Draft Parramatta Development Control Plan 2023.

TABLE 3: DPDCP 2023 PARKING REQUIREMENTS

| Land Use | Scale | Rate | Spaces Required | Spaces Provided |
| :---: | :---: | :---: | :---: | :---: |
| Child Care Centre | 90 Children | 1 per 4 children | 23 | 24 |
| TOTAL | - | - | 23 | $\mathbf{2 4}$ |

As shown, the Draft Parramatta DCP requires a minimum provision of $\mathbf{2 3}$ car parking spaces when it comes into effect. This is a lower parking requirement than that currently required by THDCP 2012. The proposed plans detail the provision of 24 car parking spaces, exceeding DPDCP 2023 parking requirements by one (1) space. It is expected that the new DCP will come into effect imminently (September 2023 according to the Project Timeline on City of Parramatta Council's website) and accordingly, the shortfall from current THDCP 2012 requirements can be disregarded in this instance. In any case, an assessment of expected visitor parking demand is provided in Section 3.1.1 below.

### 3.1.1 Car Parking Demand Analysis

In order to assess the peak demand of the child care centre parent car parking, conventional queuing theory has been employed. The results are reproduced within Annexure F with relevant details and assumptions provided below:

- An 8-minute 16 -seconds service time for each parking space (i.e. a parent uses a parking space for approximately 8-minutes 16-seconds to drop off/ pickup their child);
- This is sourced from TfNSW - Roads and Maritime Services Validation Trip Generation Survey Child Care Centres report (September 2015);
- Afternoon peak hour traffic generation of 63 trips ( $32 \mathrm{in}, 31$ out) is used as outlined within Section 4.1.

By applying conventional queuing theory, it has been determined that nine (9) car spaces can adequately accommodate the $98^{\text {th }}$ percentile parent demand in the PM peak period. The proposed plans depict ten (10) spaces dedicated for child care centre visitor use, exceeding the peak demand for the proposed use and complying with AS2890.1:2004 requirements.

### 3.2 Parking for People with Disabilities

THDCP 2012 does not outline car parking rates for people with disabilities applicable to child care centre developments. However, the DPDCP 2023 states that "The number of accessible car parking spaces to be provided as prescribed in Table D3.5 of the Building Code of Australia". It is noted that the reference to Table D3.5 refers to the 2019 version of the Building Code of Australia (BCC) which has since been superceded by Section D4D6 within the 2022 update to the National Construction Code (NCC).

As such, reference is made to the Section D4D6 of the Building Code of Australia (BCA) as part of the National Construction Code 2022 (NCC) which categorises a child care centre as a Class 9b building and therefore requires the provision of car parking for people with disabilities at a rate of:

## Class 9b 1 space for every 50 carparking spaces or part thereof.

In accordance with the BCA requirements, one (1) car parking space for people with disabilities is to be provided. The proposed car parking layout details the provision of one (1) car parking space designed in accordance with AS2890.6:2022, complying with BCA requirements.

### 3.3 Bicycle \& Motorcycle Parking Requirements

### 3.3.1 The Hills DCP 2012 Bicycle and Motorcycle Requirements

The Hills Council DCP 2012 does not require the provision of bicycle or motorcycle parking for a child care centre with a 24 space car park. Accordingly, no bicycle / motorcycle parking facilities have been provided, thus satisfying THDCP 2012 requirements.

### 3.3.2 Draft Parramatta DCP 2023 Bicycle and Motorcycle Requirements

Reference is made to the Draft Parramatta Development Control Plan 2023 (DPDCP 2023), Part 6.3 Bicycle Parking which states the following bicycle parking requirements applicable to the proposed development:
"If a particular land use is not addressed in Table 6.4.1, bicycle parking is to be provided in accordance with one of the following, whichever is the greater:

- in accordance with Austroads (2008) Guide to Traffic Management - Part 11: Parking (AGTM11-08), or
- at a rate of 0.2 spaces per car parking space that would normally be required."

It also states that:
"Unless otherwise specified, provision for motorcycle parking should be provided at a rate of 1 space per 50 car parking spaces, or part thereof."

The referenced "Austroads (2008) Guide to Traffic Management" document from the DCP has been updated to Austroads Guide to Traffic Management Part 11: Parking Management Techniques, Edition 3 published April 2020. Table 5.3 of this updated Guide includes an example of a bicycle parking provision for child care centres from Town of Cambridge, a Council in Western Australia. The requirement in Table 5.3 of this guide for a child care centre is one (1) long-stay bicycle space.

Using the other bicycle parking rate provided requires the provision of five (5) bicycle spaces (rounded from 4.6), based on the DPDCP 2023 car parking requirement of 23 spaces ( 23 x $0.2=4.6$ ). The proposed development proposes four (4) bicycle parking spaces within the basement, which exceeds the Austroads parking requirement by three (3) spaces however represents a numerical shortfall of one (1) space from the DPDCP 2023 parking rate.

With consideration for the area surrounding the site, there are no dedicated on or off-road bicycle facilities which is likely to result in travelling via bicycle to/from the centre as being undesirable for users of the child care centre. It is considered that this would be particularly undesirable for parents to children, to whom maintaining the safety of children during travel would be of the utmost importance. It is similarly expected that demand for bicycle parking from staff members would be low. Therefore, it is considered unlikely that the site will have any significant demand for bicycle parking. With consideration for the above, the proposed shortfall of one (1) space from the DPDCP 2023 bicycle parking rate requirement is considered acceptable.

Reference is made to the Draft Parramatta Development Control Plan 2023, 6.2 Parking and Vehicular Access which states the following motorcycle parking requirements applicable to the proposed development:
C. 53 Unless otherwise specified, provision for motorcycle parking should be provided at a rate of 1 space per 50 car parking spaces, or part thereof.

In accordance with the above rate, the proposed development requires the provision of one (1) motorcycle parking space. The proposed development proposes nil (0) motorcycle parking spaces, representing a numerical shortfall of one (1) space from the DPDCP 2023 requirements. It should be noted that child care centre parents/carers would not drop-off/pick-up children using a motorcycle as it is unlawful for a child under the age of 8 to be a passenger on a motorcycle in NSW. If a staff member intended on using a motorcycle to travel to/from the child care centre, the motorcycle could be stored in a staff car parking space due to the provision of one (1) car parking space per staff member in accordance with the THDCP 2012 requirements. As such, there is no need for a dedicated motorcycle space at the subject child care centre and the proposed shortfall is considered acceptable.

### 3.4 Servicing \& Loading

The THDCP 2012 and DPDCP 2023 do not outline any loading / servicing requirements applicable to a child care centre. It is expected that all deliveries will be undertaken within the proposed car parking area outside peak drop off / pick up times, under a plan of management if necessary. A van (standard B99 design vehicle) or similar can be accommodated within the car parking area, utilising vacant visitor spaces. This is common practice for child care centres and will not noticeably affect operation of the site. It is reiterated that deliveries and other arrivals of similar nature are low in frequency and can be easily managed.

It is expected that the site will be serviced by Council's waste collection services from the Mary Street frontage, similar to waste collection arrangements for the residential dwelling that currently exists onsite.

### 3.5 Car Park Design \& Compliance

The car parking layout as depicted in Annexure A, has been assessed to achieve the relevant clauses and objectives of AS2890.1:2004, AS2890.2:2018 and AS2890.6:2022. Swept path testing has been undertaken and the results are presented within Annexure G for reference.

The proposed car parking and vehicular access design achieves the following:

- Minimum 5.5 m wide two-way driveway facilitating access to Mary Street;
- Minimum 5.8 m wide parking aisles;
- Minimum 6.1 m wall-to-wall width along ramp;
- Compliant ramp grades not exceeding $25 \%$ for private developments and no grade change greater than 12.5\%;
- Minimum 5.4 m long, 2.6 m wide spaces for parents;
- Minimum 5.4 m long, 2.4 m wide accessible car parking space with adjacent associated 5.4 m long, 2.4 m wide shared space;
- Minimum headroom of 2.2 m for general circulation and 2.5 m headroom clearance provided over accessible parking areas;
- A $2.0 \mathrm{~m} \times 2.5 \mathrm{~m}$ pedestrian sight triangle on the exit side of the driveway at the property boundary which is to be kept clear of obstructions exceeding 600 mm in height for the life of the development.

Whilst the plans have been assessed to comply with the relevant standards, it is usual and expected that a design certificate be required at the Construction Certificate stage to account for any changes following the development application.

## 4 TRAFFIC ASSESSMENT

The impact of the expected traffic generation levels associated with the subject proposal is discussed in the following sub-sections.

### 4.1 Traffic Generation

Traffic generation rates for the relevant land uses are provided in the RTA Guide to Traffic Generating Developments (2002) and recent supplements as adopted by Transport for NSW (TfNSW) and are as follows:

### 3.11.3 Child care centres

Long-day care
7.00-9.00am $\quad 0.8$ peak vehicle trips per child
$2.30-4.00 \mathrm{pm} \quad 0.3$ peak vehicle trips per child
4.00-6.00pm $\quad 0.7$ peak vehicle trips per child

The resulting AM and PM peak hourly traffic generation is summarised in Table 4.
TABLE 4: ESTIMATED TRAFFIC GENERATION

| Use | Scale | Peak | Generation Rate | Trips ${ }^{(1)}$ |
| :---: | :---: | :---: | :---: | :---: |
| Long-day care | 90 Children | AM | 0.8 per child | 72 <br> $(36 ~ i n, 36 ~ o u t) ~$ |
|  |  | PM | 0.7 per child | 63 <br> $(32 \mathrm{in}, 31$ out $)$ |

Notes:
(1) $50 / 50$ inbound/outbound split.

As shown, the expected traffic generation associated with the proposed development is in the order of $\mathbf{7 2}$ vehicle trips in the AM peak period ( $36 \mathrm{in}, 36$ out) and $\mathbf{6 3}$ vehicle trips in the PM peak period (32 in, 31 out).

### 4.2 Traffic Assignment

The road network, traffic surveys and locations of residential areas surrounding the site have been assessed and the following traffic assignment has been assumed for all traffic to and from the site:

- $30 \%$ to/from the north via Windsor Road;
- $20 \%$ to/from the east via Windermere Avenue;
- $20 \%$ to/from the south via Anderson Road;
- $30 \%$ to/from the west via Windsor Road.


FIGURE 4: TRIP DISTRIBUTION

### 4.3 Traffic Impact

The traffic generation outlined in Section 4.1 \& 4.2 above has been added to the existing traffic volumes recorded. SIDRA INTERSECTION 9.1 was used to assess the intersections performance. The purpose of this assessment is to compare the existing intersection operations to the future scenario under the increased traffic load. The results of this assessment are shown in Table 5.

TABLE 5: INTERSECTION PERFORMANCE (SIDRA INTERSECTION 9.1)

| Intersection | Peak Hour | Degree of Saturation ${ }^{(1)}$ | Average Delay ${ }^{(2)}$ <br> (sec/veh) | Level of Service ${ }^{(3)(4)}$ | Control Type | Worst Movement |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EXISTING PERFORMANCE |  |  |  |  |  |  |
| Windsor Rd/ Mary St | AM | 1.03 | $\begin{gathered} 1.8 \\ \text { (Worst: >70) } \end{gathered}$ | NA <br> (Worst: F) | Give Way | RT from Windsor Rd |
|  | PM | 1.03 | $\begin{gathered} 0.8 \\ \text { (Worst: >70) } \end{gathered}$ | NA <br> (Worst: F) |  | RT from Windsor Rd |
| Margaret St / Mary St | AM | 0.05 | $3.9$ <br> (Worst: 4.9) | NA <br> (Worst: A) | Give Way | RT from Mary St |
|  | PM | 0.05 | 3.5 <br> (Worst: 4.9) | NA <br> (Worst: A) |  | RT from Mary St |
| Windermere Ave / Mary St / William St | AM | 0.05 | $2.5$ <br> (Worst: 5.1) | NA <br> (Worst: A) | Give Way | RT from Mary St / William St |
|  | PM | 0.05 | $2.1$ <br> (Worst: 5.3) | NA <br> (Worst: A) |  | RT from Mary St / William St |
| Anderson Rd / Margaret St | AM | 0.06 | $2.9$ <br> (Worst: 5.1) | NA <br> (Worst: A) | Give Way | RT from Margaret St |
|  | PM | 0.05 | $2.7$ <br> (Worst: 5.1) | NA <br> (Worst: A) |  | RT from Anderson Rd |
| Anderson Rd / Windsor Rd | AM | 0.78 | 9.6 | A | Signals | RT from Windsor Rd |
|  | PM | 0.81 | 9.7 | A |  | RT from Anderson Rd |
| FUTURE (POST-DEVELOPMENT) PERFORMANCE |  |  |  |  |  |  |
| Windsor Rd / Mary St | AM | 1.03 | $\begin{gathered} 1.8 \\ \text { (Worst: >70) } \end{gathered}$ | NA <br> (Worst: F) | Give Way | RT from Windsor Rd |
|  | PM | 1.03 | $\begin{gathered} 0.8 \\ \text { (Worst: >70) } \end{gathered}$ | NA <br> (Worst: F) |  | RT from Windsor Rd |


| Margaret St / Mary St | AM | 0.07 | $3.9$ <br> (Worst: 5.2) | NA <br> (Worst: A) | Give Way | RT from Mary St |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PM | 0.06 | $3.6$ <br> (Worst: 5.2) | NA <br> (Worst: A) |  | RT from Mary St |
| Windermere Ave / Mary St / William St | AM | 0.05 | $2.6$ <br> (Worst: 5.1) | NA <br> (Worst: A) | Give Way | RT from Mary St / William St |
|  | PM | 0.05 | $2.3$ <br> (Worst: 5.2) | NA <br> (Worst: A) |  | RT from Mary St <br> / William St |
| Anderson Rd / Margaret St | AM | 0.09 | $3.3$ <br> (Worst: 5.1) | NA <br> (Worst: A) | Give Way | RT from <br> Anderson Rd |
|  | PM | 0.07 | $3.1$ <br> (Worst: 5.1) | NA <br> (Worst: A) |  | RT from Anderson Rd |
| Anderson Rd / Windsor Rd | AM | 0.81 | 13.3 | A | Signals | RT from Windsor Rd |
|  | PM | 0.92 | 10.6 | A |  | RT from Anderson Rd |

NOTES: Refer to Table 1.
As shown, the above intersections all retain the same overall and worst movement level service under future conditions with minimal delays and additional capacity, indicating that there will be no adverse impact on the existing road network as a result of the proposed development. Whilst the Windsor Road / Mary Street intersection has a worst movement Level of Service "F", the worst movements come from turning from Mary Street onto Windsor Road and the right turn from Windsor Road into Mary Street. Realistically, parents and staff will take the fastest routes to and from the site through the intersection of Windsor Road / Anderson Road. This will not affect the intersection of Windsor Road / Mary Street.

## 5 CONCLUSION

In view of the foregoing, the subject Child Care Centre proposal at 5 Mary Street, Northmead (as depicted in Annexure A) is fully supportable in terms of its traffic and parking impacts. The following outcomes of this traffic and parking impact assessment are relevant to note:
a) The proposal includes the provision of $\mathbf{2 4}$ car parking spaces within a proposed carpark, comprised of $\mathbf{1 4}$ for staff use and 10 for visitor use, resulting in a shortfall of five (5) visitor car parking spaces from the requirements of The Hills Development Control Plan 2012 (THDCP 2012).
b) The shortfall of five (5) visitor car parking spaces from THDCP 2012 requirements is supported by queuing analysis which shows that nine (9) visitor spaces can adequately accommodate the $98^{\text {th }}$ percentile parent demand in the PM peak period. As such, the provision of ten (10) visitor car parking spaces exceeds the peak demand for the proposed use. Furthermore, it is noted that the proposed provision of 24 parking spaces satisfies the requirements of the Draft Parramatta Development Control Plan 2023 (DPDCP 2023) which is expected to come into effect during September 2023, according to the Project Timeline on the City of Parramatta Council's website.
c) THDCP 2012 does not require the provision of bicycle and motorcycle parking facilities for a child care centre. As such, nil (0) motorcycle parking spaces have been provided in plans. Four (4) bicycle parking spaces have been detailed in plans.
d) The parking areas of the site have been assessed against the relevant sections of AS2890.1:2004, AS2890.2:2018 and AS2890.6:2022 and has been found to satisfy the objectives of each standard. Swept path testing has been undertaken and the results are reproduced within Annexure G.
e) The traffic generation of the proposed development has been estimated to be some 72 trips in the AM peak period ( $36 \mathrm{in}, 36$ out) and 63 trips in the PM peak period (32 in, 31 out). The impacts of the traffic generation have been modelled using SIDRA INTERSECTION 9.1, indicating that there will be no adverse impact to the performance of the intersections as a result of the generated traffic.


## ANNEXURE A: PROPOSED PLANS

 (4 SHEETS)



$\bigcirc \frac{\text { SECTION A - }}{1.100 \text { @ Al }}$
1:100@Al



ANNEXURE B: TRAFFIC SURVEY DATA (5 SHEETS)

TURNING MOVEMENT SURVEY
Intersection of Windsor Rd and Mary St, Northmead

GPS

| GPS | $-33.778954,150.998531$ |
| :--- | :--- |
| Date: | Tue 06/06/23 |
| Weather: | Fine |
| Suburban: | Northmead |
| Customer: | McLaren |


| Survey <br> Period | AM: | 7:00 AM-9:30 AM |
| :---: | :---: | :--- |
|  | PM: | 2:30 PM-6:00 PM |
| Traffic | AM: | 7:00 AM-8:00 AM |
| Peak | PM: | 4:00 PM-5:00 PM |

All Vehicles

| Time |  | North Approach Windsor R |  |  | East Approach Mary St |  |  | pouth Approach Windsor R |  |  | Hourly Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | SB | L | U | R | L | U | R | NB | Hour | Peak |
| 7:00 | 7:15 | 0 | 490 | 0 | 0 | 0 | 2 | 0 | 0 | 279 | 3233 | Peak |
| 7:15 | 7:30 | 0 | 524 | 2 | 0 | 0 | 2 | 0 | 0 | 284 | 3231 |  |
| 7:30 | 7:45 | 0 | 526 | 1 | 0 | 0 | 2 | 0 | 0 | 317 | 3226 |  |
| 7:45 | 8:00 | 0 | 503 | 0 | 0 | 0 | 2 | 0 | 0 | 299 | 3156 |  |
| 8:00 | 8:15 | 0 | 444 | 2 | 0 | 0 | 1 | 0 | 0 | 322 | 3166 |  |
| 8:15 | 8:30 | 0 | 493 | 2 | 0 | 0 | 6 | 0 | 0 | 306 | 3182 |  |
| 8:30 | 8:45 | 0 | 471 | 4 | 0 | 2 | 9 | 0 | 0 | 290 | 3174 |  |
| 8:45 | 9:00 | 0 | 495 | 4 | 0 | 0 | 16 | 0 | 0 | 299 |  |  |
| 9:00 | 9:15 | 0 | 493 | 3 | 0 | 1 | 4 | 0 | 0 | 284 |  |  |
| 9:15 | 9:30 | 0 | 521 | 2 | 0 | 0 | 5 | 0 | 0 | 271 |  |  |
| 14:30 | 14:45 | 0 | 344 | 2 | 0 | 0 | 1 | 0 | 0 | 403 | 3420 |  |
| 14:45 | 15:00 | 0 | 393 | 2 | 0 | 2 | 4 | 0 | 0 | 444 | 3594 |  |
| 15:00 | 15:15 | 0 | 406 | 2 | 0 | 0 | 15 | 0 | 0 | 459 | 3637 |  |
| 15:15 | 15:30 | 0 | 416 | 3 | 0 | 1 | 8 | 0 | 0 | 515 | 3674 |  |
| 15:30 | 15:45 | 1 | 443 | 2 | 0 | 0 | 5 | 0 | 0 | 473 | 3683 |  |
| 15:45 | 16:00 | 0 | 400 | 6 | 0 | 1 | 5 | 0 | 0 | 476 | 3689 |  |
| 16:00 | 16:15 | 0 | 416 | 3 | 0 | 0 | 5 | 0 | 0 | 495 | 3756 | Peak |
| 16:15 | 16:30 | 0 | 442 | 4 | 0 | 0 | 0 | 0 | 0 | 506 | 3726 |  |
| 16:30 | 16:45 | 0 | 407 | 5 | 0 | 1 | 2 | 1 | 0 | 514 | 3741 |  |
| 16:45 | 17:00 | 0 | 432 | 4 | 0 | 0 | 4 | 0 | 0 | 515 | 3704 |  |
| 17:00 | 17:15 | 0 | 409 | 8 | 0 | 0 | 4 | 0 | 0 | 468 | 3655 |  |
| 17:15 | 17:30 | 0 | 475 | 3 | 0 | 0 | 1 | 0 | 0 | 488 |  |  |
| 17:30 | 17:45 | 1 | 413 | 7 | 0 | 0 | 3 | 0 | 0 | 469 |  |  |
| 17:45 | 18:00 | 0 | 459 | 3 | 0 | 0 | 2 | 0 | 0 | 442 |  |  |


| Peak Time |  | North Approach Windsor R |  |  | East Approach Mary St |  |  | pouth Approach Windsor R |  |  | Peak total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | SB | L | U | R | L | U | R | NB |  |
| 7:00 | 8:00 | 0 | 2043 | 3 | 0 | 0 | 8 | 0 | 0 | 1179 | 3233 |
| 16:00 | 17:00 | 0 | 1697 | 16 | 0 | 1 | 11 | 1 | 0 | 2030 | 3756 |

Note: Site sketch is for illustrating traffic flows. Direction is indicative only, drawing is not to scale and not an exact streets configuration.


TURNING MOVEMENT SURVEY
Intersection of Mary St and Margaret St, Northmead
GPS

| GPS | $-33.779130,150.999659$ |
| :--- | :--- |
| Date: | Tue 06/06/23 |
| Weather: | Fine |
| Suburban: | Northmead |
| Customer: | McLaren |


| North: | $\mathrm{N} / \mathrm{A}$ |
| :--- | :--- |
| East: | Mary St |
| South: | Margaret St |
| West: | Mary St |


| Survey <br> Period | AM: | 7:00 AM-9:30 AM |
| :---: | :---: | :---: |
|  | PM: | $2: 30$ PM-6:00 PM |
| Traffic | AM: | 8:15 AM-9:15 AM |
| Peak | PM: | $2: 45$ PM-3:45 PM |

All Vehicles

| Time |  | East Approach Mary St |  |  | Fouth Approach Margaret S |  |  | West Approach Mary St |  |  | Hourly Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | WB | L | U | R | L | U | R | EB | Hour | Peak |
| 7:00 | 7:15 | 0 | 2 | 6 | 0 | 5 | 0 | 0 | 0 | 0 | 55 |  |
| 7:15 | 7:30 | 0 | 2 | 5 | 0 | 3 | 0 | 0 | 1 | 1 | 67 |  |
| 7:30 | 7:45 | 0 | 2 | 8 | 0 | 7 | 0 | 0 | 0 | 1 | 99 |  |
| 7:45 | 8:00 | 0 | 2 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 111 |  |
| 8:00 | 8:15 | 0 | 0 | 14 | 0 | 8 | 1 | 0 | 0 | 2 | 146 |  |
| 8:15 | 8:30 | 1 | 5 | 17 | 0 | 18 | 1 | 0 | 2 | 0 | 150 | Peak |
| 8:30 | 8:45 | 0 | 5 | 5 | 0 | 11 | 5 | 1 | 3 | 0 | 125 |  |
| 8:45 | 9:00 | 0 | 13 | 16 | 0 | 11 | 3 | 0 | 4 | 0 |  |  |
| 9:00 | 9:15 | 0 | 3 | 14 | 0 | 7 | 2 | 0 | 2 | 1 |  |  |
| 9:15 | 9:30 | 0 | 3 | 7 | 0 | 6 | 1 | 1 | 1 | 0 |  |  |
| 14:30 | 14:45 | 0 | 0 | 5 | 0 | 11 | 1 | 0 | 0 | 2 | 125 |  |
| 14:45 | 15:00 | 0 | 6 | 7 | 0 | 10 | 0 | 0 | 0 | 2 | 135 | Peak |
| 15:00 | 15:15 | 0 | 14 | 18 | 0 | 6 | 1 | 0 | 2 | 0 | 134 |  |
| 15:15 | 15:30 | 0 | 9 | 16 | 0 | 12 | 0 | 0 | 2 | 1 | 121 |  |
| 15:30 | 15:45 | 0 | 3 | 11 | 0 | 11 | 2 | 0 | 1 | 1 | 103 |  |
| 15:45 | 16:00 | 0 | 4 | 6 | 0 | 6 | 2 | 0 | 3 | 3 | 95 |  |
| 16:00 | 16:15 | 1 | 5 | 8 | 0 | 11 | 0 | 0 | 1 | 2 | 101 |  |
| 16:15 | 16:30 | 0 | 0 | 12 | 0 | 6 | 0 | 0 | 3 | 1 | 89 |  |
| 16:30 | 16:45 | 0 | 1 | 10 | 0 | 3 | 2 | 0 | 4 | 1 | 90 |  |
| 16:45 | 17:00 | 0 | 3 | 10 | 0 | 12 | 1 | 0 | 2 | 2 | 94 |  |
| 17:00 | 17:15 | 0 | 2 | 2 | 0 | 2 | 2 | 0 | 6 | 2 | 85 |  |
| 17:15 | 17:30 | 0 | 0 | 7 | 0 | 12 | 1 | 0 | 3 | 0 |  |  |
| 17:30 | 17:45 | 0 | 3 | 6 | 0 | 9 | 0 | 0 | 5 | 2 |  |  |
| 17:45 | 18:00 | 0 | 2 | 2 | 1 | 13 | 0 | 0 | 0 | 3 |  |  |


| Peak Time |  | East Approach Mary St |  |  | Fouth Approach Margaret S |  |  | West Approach Mary St |  |  | $\begin{aligned} & \hline \text { Peak } \\ & \text { total } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | WB | L | U | R | L | U | R | EB |  |
| 8:15 | 9:15 | 1 | 26 | 52 | 0 | 47 | 11 | 1 | 11 | 1 | 150 |
| 14:45 | 15:45 | 0 | 32 | 52 | 0 | 39 | 3 | 0 | 5 | 4 | 135 |

Note: Site sketch is for illustrating traffic flows. Direction is indicative only, drawing is not to scale and not an exact streets configuration. Graphic
$\frac{\text { Graphic }}{\text { Total }}$
Light
Heavy


## TRANS TRAFFIC SURVEY

$\overline{\text { ONV.GL }}$
$\overline{\overline{\text { ONV.GL }}}$
$\overline{\overline{O N V} \cdot G L}$
TURNING MOVEMENT SURVEY
Mafficsurvey.com.au

(even
(soo
Intersection of Windermere Ave and William St, Northme
GPS

| GPS | $-33.778237,151.003137$ |
| :--- | :--- |
| Date: | Tue 06/06/23 |
| Weather: | Fine |
| Suburban: | Northmead |
| Customer: | McLaren |


| North: | N/A |
| :--- | :--- |
| East: | Windermere Ave |
| South: | William St |
| West: | Windermere Ave |


| Survey <br> Period | AM: | 7:00 AM-9:30 AM |
| :---: | :---: | :---: |
|  | PM: | $2: 30$ PM-6:00 PM |
| Traffic <br> Peak | AM: | 8:00 AM-9:00 AM |
|  | PM: | $3: 15$ PM-4:15 PM |

All Vehicles

| Time |  | st Approach Windermere ASouth Approach William Stst Approach Windermere A |  |  |  |  |  |  |  |  | Hourly Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | WB | L | U | R | L | U | R | EB | Hour | Peak |
| 7:00 | 7:15 | 1 | 6 | 5 | 0 | 1 | 3 | 0 | 3 | 7 | 110 |  |
| 7:15 | 7:30 | 1 | 2 | 6 | 0 | 1 | 0 | 1 | 2 | 12 | 130 |  |
| 7:30 | 7:45 | 0 | 9 | 3 | 1 | 1 | 3 | 0 | 3 | 11 | 159 |  |
| 7:45 | 8:00 | 0 | 10 | 2 | 0 | 0 | 3 | 1 | 3 | 9 | 171 |  |
| 8:00 | 8:15 | 0 | 11 | 5 | 1 | 1 | 1 | 0 | 12 | 15 | 189 | Peak |
| 8:15 | 8:30 | 0 | 8 | 11 | 0 | 3 | 8 | 0 | 8 | 16 | 176 |  |
| 8:30 | 8:45 | 0 | 14 | 7 | 1 | 2 | 3 | 0 | 7 | 9 | 149 |  |
| 8:45 | 9:00 | 0 | 8 | 9 | 0 | 2 | 3 | 0 | 12 | 12 |  |  |
| 9:00 | 9:15 | 0 | 2 | 5 | 0 | 1 | 4 | 0 | 3 | 18 |  |  |
| 9:15 | 9:30 | 0 | 9 | 1 | 0 | 0 | 4 | 1 | 5 | 7 |  |  |
| 14:30 | 14:45 | 0 | 4 | 2 | 0 | 2 | 2 | 0 | 2 | 7 | 124 |  |
| 14:45 | 15:00 | 0 | 7 | 7 | 0 | 1 | 4 | 0 | 5 | 7 | 147 |  |
| 15:00 | 15:15 | 0 | 6 | 1 | 0 | 2 | 4 | 0 | 0 | 5 | 148 |  |
| 15:15 | 15:30 | 0 | 13 | 1 | 0 | 0 | 11 | 1 | 13 | 17 | 183 | Peak |
| 15:30 | 15:45 | 0 | 5 | 4 | 1 | 3 | 8 | 0 | 2 | 19 | 176 |  |
| 15:45 | 16:00 | 1 | 9 | 2 | 0 | 2 | 6 | 0 | 4 | 8 | 168 |  |
| 16:00 | 16:15 | 0 | 12 | 10 | 0 | 1 | 5 | 0 | 4 | 21 | 178 |  |
| 16:15 | 16:30 | 0 | 13 | 2 | 0 | 1 | 5 | 0 | 8 | 20 | 167 |  |
| 16:30 | 16:45 | 0 | 5 | 1 | 0 | 1 | 7 | 0 | 4 | 16 | 157 |  |
| 16:45 | 17:00 | 0 | 12 | 0 | 0 | 1 | 6 | 0 | 6 | 17 | 160 |  |
| 17:00 | 17:15 | 0 | 7 | 2 | 0 | 4 | 2 | 0 | 7 | 20 | 174 |  |
| 17:15 | 17:30 | 0 | 9 | 1 | 0 | 1 | 8 | 0 | 0 | 20 |  |  |
| 17:30 | 17:45 | 0 | 9 | 0 | 0 | 4 | 5 | 0 | 5 | 14 |  |  |
| 17:45 | 18:00 | 0 | 24 | 2 | 0 | 4 | 8 | 0 | 6 | 12 |  |  |


| Peak Time |  | st Approach Windermere ASouth Approach William Stst Approach Windermere A |  |  |  |  |  |  |  |  | Peak total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | WB | L | U | R | L | U | R | EB |  |
| 8:00 | 9:00 | 0 | 41 | 32 | 2 | 8 | 15 | 0 | 39 | 52 | 189 |
| 15:15 | 16:15 | 1 | 39 | 17 | 1 | 6 | 30 | 1 | 23 | 65 | 183 |

Note: Site sketch is for illustrating traffic flows. Direction is indicative only, drawing is not to scale and not an exact streets configuration.

| Graphic |
| :---: |
| Total |
| Light |
| Heavy |




Intersection of Anderson Rd and Margaret St, Northmea
GPS

| Date: | Tue 06/06/23 |
| :--- | :--- |
| Weather: | Fine |
| Suburban: | Northmead |
| Customer: | McLaren |


| North: | Margaret St |
| :--- | :--- |
| East: | Anderson Rd |
| South: | N/A |
| West: | Anderson Rd |


| Survey | AM: | $7: 00$ AM-9:30 AM |
| :---: | :---: | :--- |
| Period | $\mathrm{PM}:$ | $2: 30$ PM-6:00 PM |
| Traffic | $\mathrm{AM}:$ | 8:00 AM-9:00 AM |
| Peak | PM: | $4: 00$ PM-5:00 PM |


| Time |  | North Approach Margaret SE |  |  | East Approach Anderson R\Vest Approach Anderson R |  |  |  |  |  | Hourly Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | R | L | U | R | WB | U | EB | L | Hour | Peak |
| 7:00 | 7:15 | 0 | 6 | 0 | 0 | 0 | 5 | 0 | 0 | 6 | 142 |  |
| 7:15 | 7:30 | 1 | 9 | 1 | 0 | 2 | 18 | 0 | 2 | 4 | 174 |  |
| 7:30 | 7:45 | 0 | 6 | 3 | 0 | 1 | 26 | 0 | 6 | 7 | 203 |  |
| 7:45 | 8:00 | 0 | 7 | 3 | 0 | 2 | 18 | 0 | 4 | 5 | 212 |  |
| 8:00 | 8:15 | 0 | 15 | 1 | 0 | 3 | 17 | 0 | 3 | 10 | 224 | Peak |
| 8:15 | 8:30 | 0 | 17 | 4 | 0 | 4 | 21 | 0 | 2 | 18 | 220 |  |
| 8:30 | 8:45 | 1 | 8 | 4 | 0 | 6 | 22 | 1 | 5 | 11 | 183 |  |
| 8:45 | 9:00 | 0 | 12 | 8 | 0 | 2 | 12 | 0 | 6 | 11 |  |  |
| 9:00 | 9:15 | 1 | 13 | 5 | 0 | 4 | 8 | 0 | 8 | 6 |  |  |
| 9:15 | 9:30 | 0 | 9 | 1 | 0 | 2 | 8 | 0 | 2 | 7 |  |  |
| 14:30 | 14:45 | 0 | 4 | 2 | 0 | 2 | 7 | 0 | 8 | 13 | 173 |  |
| 14:45 | 15:00 | 0 | 10 | 2 | 1 | 1 | 15 | 0 | 4 | 10 | 176 |  |
| 15:00 | 15:15 | 0 | 19 | 2 | 0 | 1 | 12 | 0 | 4 | 5 | 170 |  |
| 15:15 | 15:30 | 0 | 16 | 4 | 0 | 1 | 8 | 0 | 9 | 13 | 184 |  |
| 15:30 | 15:45 | 0 | 8 | 2 | 0 | 3 | 8 | 1 | 5 | 12 | 176 |  |
| 15:45 | 16:00 | 0 | 10 | 2 | 0 | 0 | 9 | 2 | 4 | 10 | 183 |  |
| 16:00 | 16:15 | 0 | 13 | 3 | 0 | 3 | 14 | 1 | 11 | 12 | 193 | Peak |
| 16:15 | 16:30 | 0 | 12 | 3 | 0 | 3 | 11 | 0 | 6 | 8 | 173 |  |
| 16:30 | 16:45 | 0 | 13 | 2 | 0 | 1 | 11 | 0 | 12 | 7 | 174 |  |
| 16:45 | 17:00 | 0 | 10 | 3 | 0 | 2 | 10 | 0 | 11 | 11 | 174 |  |
| 17:00 | 17:15 | 0 | 7 | 2 | 0 | 2 | 16 | 0 | 2 | 8 | 156 |  |
| 17:15 | 17:30 | 0 | 7 | 2 | 0 | 0 | 12 | 0 | 9 | 14 |  |  |
| 17:30 | 17:45 | 0 | 8 | 1 | 0 | 2 | 10 | 1 | 12 | 12 |  |  |
| 17:45 | 18:00 | 0 | 3 | 1 | 0 | 2 | 3 | 1 | 7 | 12 |  |  |


| Peak Time |  | North Approach Margaret SEast Approach Anderson R(Vest Approach Anderson R | Peak |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | $U$ | R | L | U | R | WB | U | EB | L | total |
| $8: 00$ | $9: 00$ | 1 | 52 | 17 | 0 | 15 | 72 | 1 | 16 | 50 | 224 |
| $16: 00$ | $17: 00$ | 0 | 48 | 11 | 0 | 9 | 46 | 1 | 40 | 38 | 193 |



TRANS TRAFFIC SURVEY
TURNING MOVEMENT SURVEY
Intersection of Anderson Rd and Windsor Rd, Northmead

| GPS | $-33.781983,150.996831$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Date: | Tue 06/06/23 |
| Weather: | Fine |
| Suburban: | Northmead |
| Customer: | McLaren |


| Time |  | North Approach Windsor Rd |  |  |  | East Approach Anderson Rd |  |  |  | South Approach Windsor Rd |  |  |  | West Approach Club Access |  |  |  | Hourly Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Star | Period End | $U$ | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L | Hour | Peak |
| 7:00 | 7:15 | 0 | 0 | 609 | 4 | 0 | 10 | 0 | 2 | 0 | 3 | 266 | 0 | 0 | 0 | 0 | 0 | 3755 |  |
| 7:15 | 7:30 | 0 | 0 | 635 | 4 | 0 | 21 | 2 | 6 | 0 | 1 | 266 | 0 | 0 | 0 | 2 | 0 | 3773 | Peak |
| 7:30 | 7:45 | 0 | 0 | 663 | 5 | 0 | 25 | 2 | 7 | 0 | 2 | 267 | 0 | 0 | 0 | 4 | 0 | 3749 |  |
| 7:45 | 8:00 | 0 | 0 | 647 | 7 | 0 | 18 | 0 | 5 | 0 | 2 | 268 | 0 | 0 | 2 | 0 | 0 | 3620 |  |
| 8:00 | 8:15 | 0 | 0 | 599 | 5 | 0 | 25 | 0 | 5 | 0 | 8 | 270 | 0 | 0 | 0 | 0 | 0 | 3559 |  |
| 8:15 | 8:30 | 0 | 0 | 600 | 13 | 0 | 23 | 1 | 8 | 0 | 8 | 260 | 0 | 0 | 0 | 0 | 0 | 3489 |  |
| 8:30 | 8:45 | 0 | 0 | 586 | 7 | 0 | 25 | 2 | 4 | 0 | 8 | 214 | 0 | 0 | 0 | 0 | 0 | 3433 |  |
| 8:45 | 9:00 | 0 | 0 | 595 | 8 | 0 | 19 | 0 | 4 | 0 | 7 | 255 | 0 | 0 | 0 | 0 | 0 |  |  |
| 9:00 | 9:15 | 0 | 0 | 560 | 12 | 0 | 20 | 2 | 8 | 0 | 4 | 236 | 0 | 0 | 0 | 0 | 0 |  |  |
| 9:15 | 9:30 | 0 | 0 | 580 | 6 | 0 | 15 | 0 | 4 | 0 | 4 | 248 | 0 | 0 | 0 | 0 | 0 |  |  |
| 14:30 | 14:45 | 0 | 0 | 356 | 6 | 0 | 10 | 0 | 3 | 0 | 13 | 438 | 0 | 0 | 0 | 0 | 0 | 3658 |  |
| 14:45 | 15:00 | 0 | 0 | 411 | 9 | 0 | 19 | 0 | 7 | 0 | 4 | 463 | 0 | 0 | 0 | 0 | 0 | 3870 |  |
| 15:00 | 15:15 | 0 | 0 | 443 | 9 | 0 | 22 | 0 | 5 | 0 | 1 | 465 | 0 | 0 | 1 | 0 | 0 | 3902 |  |
| 15:15 | 15:30 | 0 | 0 | 406 | 14 | 0 | 22 | 1 | 5 | 1 | 10 | 510 | 0 | 0 | 4 | 0 | 0 | 3974 |  |
| 15:30 | 15:45 | 0 | 0 | 506 | 8 | 0 | 13 | 0 | 2 | 0 | 9 | 500 | 0 | 0 | 0 | 0 | 0 | 4040 |  |
| 15:45 | 16:00 | 0 | 0 | 388 | 8 | 0 | 21 | 2 | 4 | 0 | 8 | 512 | 0 | 0 | 2 | 0 | 0 | 3985 |  |
| 16:00 | 16:15 | 0 | 0 | 460 | 16 | 0 | 22 | 2 | 3 | 0 | 5 | 506 | 0 | 0 | 3 | 1 | 0 | 4102 | Peak |
| 16:15 | 16:30 | 0 | 0 | 471 | 9 | 0 | 18 | 3 | 1 | 0 | 4 | 533 | 0 | 0 | 0 | 0 | 0 | 4046 |  |
| 16:30 | 16:45 | 0 | 0 | 408 | 12 | 0 | 22 | 1 | 3 | 0 | 4 | 530 | 0 | 0 | 2 | 1 | 0 | 4079 |  |
| 16:45 | 17:00 | 0 | 0 | 473 | 16 | 0 | 21 | 0 | 1 | 0 | 9 | 540 | 1 | 0 | 1 | 0 | 0 | 4051 |  |
| 17:00 | 17:15 | 0 | 0 | 425 | 7 | 0 | 17 | 1 | 2 | 0 | 5 | 504 | 0 | 0 | 1 | 0 | 0 | 4051 |  |
| 17:15 | 17:30 | 0 | 0 | 527 | 17 | 0 | 14 | 1 | 1 | 0 | 5 | 507 | 0 | 0 | 0 | 0 | 0 |  |  |
| 17:30 | 17:45 | 0 | 0 | 412 | 17 | 0 | 16 | 2 | 4 | 0 | 10 | 494 | 0 | 0 | 0 | 0 | 0 |  |  |
| 17:45 | 18:00 | 0 | 0 | 532 | 16 | 0 | 10 | 0 | 2 | 0 | 4 | 498 | 0 | 0 | 0 | 0 | 0 |  |  |


| Peak Time |  | North Approach Windsor Rd |  |  |  | East Approach Anderson Rd |  |  |  | South Approach Windsor Rd |  |  |  | West Approach Club Access |  |  |  | Peak total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Star | Period End | U | R | SB | L | U | R | WB | L | U | R | NB | L | U | R | EB | L |  |
| 7:15 | 8:15 | 0 | 0 | 2544 | 21 | 0 | 89 | 4 | 23 | 0 | 13 | 1071 | 0 | 0 | 2 | 6 | 0 | 3773 |
| 16:00 | 17:00 | 0 | 0 | 1812 | 53 | 0 | 83 | 6 | 8 | 0 | 22 | 2109 | 1 | 0 | 6 | 2 | 0 | 4102 |




ANNEXURE C: SIDRA RESULTS (20 SHEETS)

## MOVEMENT SUMMARY

## $\nabla$ Site: 1 [(ExAM) Windsor Rd / Mary St (Site Folder: Existing)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Windsor Rd / Mary St
Existing AM Peak
Job No 220918
Site Category: Existing AM
Give-Way (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:24 PM
Project: Z:\Jobs\2022\220918\MTE SIDRAl23 0718 - KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 4 [(ExAM) Anderson Rd / Margaret St (Site Folder: <br> Existing)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Anderson Rd / Margaret St
Existing AM Peak
Job No 220918
Site Category: Existing AM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Mov Class | $\begin{array}{r} \text { Dem } \\ \text { F } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { nand } \\ \text { lows } \\ \text { HV ] } \\ \% \end{gathered}$ | Ar Fl Total veh/h | $\begin{aligned} & \text { rrival } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{array}{r} 95 \% \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{array}$ | $\begin{gathered} \text { ck Of } \\ \text { ue } \\ \text { Dist ] } \\ m \end{gathered}$ | Prop. Que | $\begin{aligned} & \text { Eff. } \\ & \text { Stop } \\ & \text { Rate } \end{aligned}$ | Aver. No. of Cycles | Aver. Speed <br> km/h |
| East: Anderson Rd (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | All MCs | 76 | 1.4 | 76 | 1.4 | 0.049 | 0.0 | LOS A | 0.1 | 0.7 | 0.06 | 0.11 | 0.06 | 48.9 |
| 6 | R2 | All MCs | 16 | 0.0 | 16 | 0.0 | 0.049 | 5.0 | LOS A | 0.1 | 0.7 | 0.06 | 0.11 | 0.06 | 47.9 |
| Appr | ach |  | 92 | 1.1 | 92 | 1.1 | 0.049 | 0.9 | NA | 0.1 | 0.7 | 0.06 | 0.11 | 0.06 | 48.7 |
| North: Margaret St (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 18 | 0.0 | 18 | 0.0 | 0.060 | 4.6 | LOS A | 0.2 | 1.5 | 0.13 | 0.52 | 0.13 | 45.7 |
| 9 | R2 | All MCs | 56 | 1.9 | 56 | 1.9 | 0.060 | 5.1 | LOS A | 0.2 | 1.5 | 0.13 | 0.52 | 0.13 | 43.5 |
| Appr | ach |  | 74 | 1.4 | 74 | 1.4 | 0.060 | 5.0 | LOS A | 0.2 | 1.5 | 0.13 | 0.52 | 0.13 | 44.2 |
| West: Anderson Rd (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | All MCs | 54 | 2.0 | 54 | 2.0 | 0.038 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 45.0 |
| 11 | T1 | All MCs | 17 | 0.0 | 17 | 0.0 | 0.038 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 46.7 |
| Approach |  |  | 71 | 1.5 | 71 | 1.5 | 0.038 | 3.5 | NA | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 45.4 |
| All Vehicles |  |  | 236 | 1.3 | 236 | 1.3 | 0.060 | 2.9 | NA | 0.2 | 1.5 | 0.06 | 0.33 | 0.06 | 46.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:28 PM
Project: Z:\Jobs\2022l220918\MTE SIDRAI23 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 1 [(ExPM) Windsor Rd / Mary St (Site Folder: Existing)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Windsor Rd / Mary St
Existing PM Peak
Job No 220918
Site Category: Existing PM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn Mov  <br> ID Class |  | $\begin{aligned} & \text { nand } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | rival lows HV ] \% | Deg. Satn $\qquad$ v/c | Aver. Delay $\qquad$ sec | Level of Service | 95\% <br> Q <br> [ Veh. veh | $\begin{gathered} \text { ck Of } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que |  | Aver. No. of Cycles | Aver. Speed $\qquad$ km/h |
| South: Windsor Rd (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 All MCs | 2137 | 2.7 | 2137 | 2.7 | 0.564 | 0.1 | LOS A | 0.4 | 2.7 | 0.01 | 0.01 | 0.01 | 59.5 |
| 3 R2 All MCs | 1 | 0.0 | 1 | 0.0 | 0.564 | 352.9 | LOS F | 0.4 | 2.7 | 0.01 | 0.01 | 0.01 | 51.6 |
| Approach | 2138 | 2.7 | 2138 | 2.7 | 0.564 | 0.3 | NA | 0.4 | 2.7 | 0.01 | 0.01 | 0.01 | 59.5 |
| East: Mary St (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 All MCs | 12 | 0.0 | 12 | 0.0 | 1.029 | 169.1 | LOS F | 2.2 | 15.7 | 1.00 | 1.02 | 1.19 | 14.3 |
| 6 R2 All MCs | 1 | 0.0 | 1 | 0.0 | 1.029 | 65.4 | LOS E | 2.2 | 15.7 | 1.00 | 1.02 | 1.19 | 15.9 |
| Approach | 13 |  | 13 |  | 1.029 | 160.5 | LOS F | 2.2 | 15.7 | 1.00 | 1.02 | 1.19 | 14.4 |
| North: Windsor Rd (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 All MCs | 17 | 0.0 | 17 | 0.0 | 0.479 | 5.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 57.1 |
| 8 T1 All MCs | 1786 | 5.5 | 1786 | 5.5 | 0.479 | 0.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 59.6 |
| Approach | 1803 | 5.5 | 1803 | 5.5 | 0.479 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 59.5 |
| All Vehicles | 3954 | 3.9 | 3954 |  | 1.029 | 0.8 | NA | 2.2 | 15.7 | 0.01 | 0.01 | 0.01 | 58.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:25 PM
Project: Z:\Jobs\2022\220918\MTE SIDRAl23 0718 - KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 2 [(ExAM) Mary St / Margaret St (Site Folder: Existing)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

```
Mary St / Margaret St
Existing AM Peak
Job No 220918
Site Category: Existing AM
Give-Way (Two-Way)
```

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn Mov ID Class | Dem Flo [ Total veh/h |  | $\begin{array}{r} \text { Arı } \\ \text { Fl } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | rival lows HV ] \% | Deg. Satn $\qquad$ v/c | Aver. Delay $\qquad$ sec | Level of Service |  | ck Of ue Dist ] m | Prop. Que |  | Aver. No. of Cycles | Aver. Speed $\qquad$ km/h |
| South: Margaret St (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 All MCs | 13 | 0.0 | 13 | 0.0 | 0.049 | 4.6 | LOS A | 0.2 | 1.2 | 0.12 | 0.53 | 0.12 | 45.7 |
| 3 R2 All MCs | 49 |  | 49 |  | 0.049 | 4.8 | LOS A | 0.2 | 1.2 | 0.12 | 0.53 | 0.12 | 45.5 |
| Approach | 62 | 1.7 | 62 | 1.7 | 0.049 | 4.8 | LOS A | 0.2 | 1.2 | 0.12 | 0.53 | 0.12 | 45.5 |
| East: Mary St (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 All MCs | 55 | 0.0 | 55 | 0.0 | 0.044 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.36 | 0.00 | 46.8 |
| 5 T1 All MCs | 27 | 0.0 | 27 |  | 0.044 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.36 | 0.00 | 48.0 |
| Approach | 82 | 0.0 | 82 | 0.0 | 0.044 | 3.1 | NA | 0.0 | 0.0 | 0.00 | 0.36 | 0.00 | 47.2 |
| West: Mary St (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 All MCs | 1 | 0.0 | 1 | 0.0 | 0.008 | 0.0 | LOS A | 0.0 | 0.3 | 0.18 | 0.48 | 0.18 | 46.9 |
| 12 R2 All MCs | 13 |  | 13 |  | 0.008 | 4.9 | LOS A | 0.0 | 0.3 | 0.18 | 0.48 | 0.18 | 45.5 |
| Approach | 14 |  | 14 |  | 0.008 | 4.5 | NA | 0.0 | 0.3 | 0.18 | 0.48 | 0.18 | 45.6 |
| All Vehicles | 158 | 1.3 | 158 | 1.3 | 0.049 | 3.9 | NA | 0.2 | 1.2 | 0.06 | 0.43 | 0.06 | 46.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:26 PM
Project: Z:\Jobs\2022\220918\MTE SIDRAl23 0718 - KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 2 [(ExPM) Mary St / Margaret St (Site Folder: Existing)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

```
Mary St / Margaret St
Existing PM Peak
Job No 220918
Site Category: Existing PM
Give-Way (Two-Way)
```

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn Mov ID Class | Dem Flo [ Total veh/h |  | $\begin{gathered} \text { Arr } \\ \text { Flc } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | rival lows HV ] \% | Deg. Satn $\qquad$ v/c | Aver. Delay $\qquad$ sec | Level of Service |  | ck Of ue Dist ] m | Prop. Que |  | Aver. No. of Cycles | Aver. Speed $\qquad$ km/h |
| South: Margaret St (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 All MCs | 3 | 0.0 | 3 | 0.0 | 0.036 | 4.7 | LOS A | 0.1 | 0.8 | 0.14 | 0.53 | 0.14 | 45.7 |
| 3 R2 All MCs | 41 |  | 41 |  | 0.036 | 4.8 | LOS A | 0.1 | 0.8 | 0.14 | 0.53 | 0.14 | 45.4 |
| Approach | 44 |  | 44 |  | 0.036 | 4.8 | LOS A | 0.1 | 0.8 | 0.14 | 0.53 | 0.14 | 45.4 |
| East: Mary St (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 All MCs | 55 |  | 55 | 1.9 | 0.048 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.33 | 0.00 | 46.9 |
| 5 T1 All MCs | 34 |  | 34 |  | 0.048 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.33 | 0.00 | 48.1 |
| Approach | 88 |  | 88 |  | 0.048 | 2.8 | NA | 0.0 | 0.0 | 0.00 | 0.33 | 0.00 | 47.4 |
| West: Mary St (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 All MCs | 4 |  | 4 | 0.0 | 0.005 | 0.0 | LOS A | 0.0 | 0.2 | 0.17 | 0.31 | 0.17 | 47.9 |
| 12 R2 All MCs | 5 | 0.0 | 5 |  | 0.005 | 4.9 | LOS A | 0.0 | 0.2 | 0.17 | 0.31 | 0.17 | 46.6 |
| Approach | 9 | 0.0 | 9 |  | 0.005 | 2.7 | NA | 0.0 | 0.2 | 0.17 | 0.31 | 0.17 | 47.1 |
| All Vehicles | 142 | 2.2 | 142 |  | 0.048 | 3.5 | NA | 0.1 | 0.8 | 0.05 | 0.39 | 0.05 | 46.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:26 PM
Project: Z:\Jobs\2022\220918\MTE SIDRAl23 0718 - KL - LS Edits.sip9

## MOVEMENT SUMMARY

$\nabla$ Site: 3 [(ExAM) William St / Windermere Ave (Site Folder:
Existing)]
Output produced by SIDRA INTERSECTION Version: 9.1.3.210
William St / Windermere Ave
Existing AM Peak
Job No 220918
Site Category: Existing AM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID |  | Mov Class | Dem Fl <br> [ Total veh/h | mand ows HV ] \% |  | rival ows HV ] \% | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | ck Of e Dist ] m | Prop. Que | Eff. <br> Stop <br> Rate | Aver. No. of Cycles | Aver. Speed <br> km/h |
| South: Mary St / William St (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | All MCs | 16 | 0.0 | 16 | 0.0 | 0.019 | 4.7 | LOS A | 0.1 | 0.5 | 0.14 | 0.51 | 0.14 | 45.7 |
| 3 | R2 | All MCs | 11 | 0.0 | 11 | 0.0 | 0.019 | 5.1 | LOS A | 0.1 | 0.5 | 0.14 | 0.51 | 0.14 | 45.5 |
| Appr | ach |  | 26 | 0.0 | 26 | 0.0 | 0.019 | 4.8 | LOS A | 0.1 | 0.5 | 0.14 | 0.51 | 0.14 | 45.6 |
| East: Windermere Ave (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | All MCs | 36 | 0.0 | 36 | 0.0 | 0.041 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.25 | 0.00 | 47.4 |
| 5 | T1 | All MCs | 43 | 0.0 | 43 | 0.0 | 0.041 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.25 | 0.00 | 48.6 |
| Approach |  |  | 79 | 0.0 | 79 | 0.0 | 0.041 | 2.1 | NA | 0.0 | 0.0 | 0.00 | 0.25 | 0.00 | 48.1 |
| West: Windermere Ave (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | All MCs | 55 | 5.8 | 55 | 5.8 | 0.054 | 0.0 | LOS A | 0.2 | 1.5 | 0.14 | 0.25 | 0.14 | 48.3 |
| 12 | R2 | All MCs | 41 | 0.0 | 41 |  | 0.054 | 5.0 | LOS A | 0.2 | 1.5 | 0.14 | 0.25 | 0.14 | 46.9 |
| Appr |  |  | 96 |  | 96 | 3.3 | 0.054 | 2.1 | NA | 0.2 | 1.5 | 0.14 | 0.25 | 0.14 | 47.7 |
| All V | icles |  | 201 | 1.6 | 201 | 1.6 | 0.054 | 2.5 | NA | 0.2 | 1.5 | 0.09 | 0.28 | 0.09 | 47.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:27 PM
Project: Z:\Jobs\2022l220918\MTE SIDRAl23 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 3 [(ExPM) William St / Windermere Ave (Site Folder: <br> Existing)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
William St / Windermere Ave
Existing PM Peak
Job No 220918
Site Category: Existing PM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID |  | Mov Class | Dem Fl <br> [ Total veh/h | mand ows HV ] \% |  | rival ows HV ] \% | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | ck Of e Dist ] m | Prop. Que | Eff. <br> Stop <br> Rate | Aver. No. of Cycles | Aver. Speed <br> km/h |
| South: Mary St / William St (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | All MCs | 33 |  | 33 | 0.0 | 0.028 | 4.7 | LOS A | 0.1 | 0.8 | 0.12 | 0.50 | 0.12 | 45.7 |
| 3 | R2 | All MCs |  | 14.3 |  | 14.3 | 0.028 | 5.3 | LOS A | 0.1 | 0.8 | 0.12 | 0.50 | 0.12 | 45.3 |
| Appr | ach |  | 40 |  | 40 | 2.6 | 0.028 | 4.8 | LOS A | 0.1 | 0.8 | 0.12 | 0.50 | 0.12 | 45.6 |
| East: Windermere Ave (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | All MCs | 18 | 5.9 | 18 | 5.9 | 0.031 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.16 | 0.00 | 47.8 |
| 5 | T1 | All MCs | 41 |  | 41 |  | 0.031 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.16 | 0.00 | 49.1 |
| Approach |  |  | 59 | 3.6 | 59 | 3.6 | 0.031 | 1.4 | NA | 0.0 | 0.0 | 0.00 | 0.16 | 0.00 | 48.7 |
| West: Windermere Ave (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | All MCs | 68 | 3.1 | 68 | 3.1 | 0.051 | 0.0 | LOS A | 0.1 | 1.0 | 0.09 | 0.16 | 0.09 | 48.9 |
| 12 | R2 | All MCs | 25 |  | 25 |  | 0.051 | 4.9 | LOS A | 0.1 | 1.0 | 0.09 | 0.16 | 0.09 | 47.5 |
| Appr | ach |  | 94 |  | 94 |  | 0.051 | 1.3 | NA | 0.1 | 1.0 | 0.09 | 0.16 | 0.09 | 48.5 |
| All V | icles |  | 193 | 2.7 | 193 | 2.7 | 0.051 | 2.1 | NA | 0.1 | 1.0 | 0.07 | 0.23 | 0.07 | 47.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:28 PM
Project: Z:\Jobs\2022l220918\MTE SIDRAl23 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 4 [(ExAM) Anderson Rd / Margaret St (Site Folder: <br> Existing)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Anderson Rd / Margaret St
Existing AM Peak
Job No 220918
Site Category: Existing AM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Mov Class | $\begin{array}{r} \text { Dem } \\ \text { F } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { nand } \\ \text { lows } \\ \text { HV ] } \\ \% \end{gathered}$ | Ar Fl Total veh/h | $\begin{aligned} & \text { rrival } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{array}{r} 95 \% \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{array}$ | $\begin{gathered} \text { ck Of } \\ \text { ue } \\ \text { Dist ] } \\ m \end{gathered}$ | Prop. Que | $\begin{aligned} & \text { Eff. } \\ & \text { Stop } \\ & \text { Rate } \end{aligned}$ | Aver. No. of Cycles | Aver. Speed <br> km/h |
| East: Anderson Rd (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | All MCs | 76 | 1.4 | 76 | 1.4 | 0.049 | 0.0 | LOS A | 0.1 | 0.7 | 0.06 | 0.11 | 0.06 | 48.9 |
| 6 | R2 | All MCs | 16 | 0.0 | 16 | 0.0 | 0.049 | 5.0 | LOS A | 0.1 | 0.7 | 0.06 | 0.11 | 0.06 | 47.9 |
| Appr | ach |  | 92 | 1.1 | 92 | 1.1 | 0.049 | 0.9 | NA | 0.1 | 0.7 | 0.06 | 0.11 | 0.06 | 48.7 |
| North: Margaret St (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 18 | 0.0 | 18 | 0.0 | 0.060 | 4.6 | LOS A | 0.2 | 1.5 | 0.13 | 0.52 | 0.13 | 45.7 |
| 9 | R2 | All MCs | 56 | 1.9 | 56 | 1.9 | 0.060 | 5.1 | LOS A | 0.2 | 1.5 | 0.13 | 0.52 | 0.13 | 43.5 |
| Appr | ach |  | 74 | 1.4 | 74 | 1.4 | 0.060 | 5.0 | LOS A | 0.2 | 1.5 | 0.13 | 0.52 | 0.13 | 44.2 |
| West: Anderson Rd (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | All MCs | 54 | 2.0 | 54 | 2.0 | 0.038 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 45.0 |
| 11 | T1 | All MCs | 17 | 0.0 | 17 | 0.0 | 0.038 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 46.7 |
| Approach |  |  | 71 | 1.5 | 71 | 1.5 | 0.038 | 3.5 | NA | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 45.4 |
| All Vehicles |  |  | 236 | 1.3 | 236 | 1.3 | 0.060 | 2.9 | NA | 0.2 | 1.5 | 0.06 | 0.33 | 0.06 | 46.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:28 PM
Project: Z:\Jobs\2022l220918\MTE SIDRAI23 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 4 [(ExPM) Anderson Rd / Margaret St (Site Folder: <br> Existing)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Anderson Rd / Margaret St
Existing PM Peak
Job No 220918
Site Category: Existing PM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Mov Class | $\begin{array}{r} \text { Dem } \\ \text { F } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { nand } \\ \text { lows } \\ \text { HV ] } \\ \% \end{gathered}$ | Ar Fl Total veh/h | $\begin{aligned} & \text { rrival } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{array}{r} 95 \% \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{array}$ | $\begin{gathered} \text { ck Of } \\ \text { ue } \\ \text { Dist ] } \\ m \end{gathered}$ | Prop. Que | $\begin{aligned} & \text { Eff. } \\ & \text { Stop } \\ & \text { Rate } \end{aligned}$ | Aver. No. of Cycles | Aver. Speed <br> km/h |
| East: Anderson Rd (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | All MCs | 48 | 2.2 | 48 | 2.2 | 0.031 | 0.0 | LOS A | 0.1 | 0.4 | 0.07 | 0.11 | 0.07 | 49.0 |
| 6 | R2 | All MCs | 9 | 0.0 | 9 | 0.0 | 0.031 | 5.1 | LOS A | 0.1 | 0.4 | 0.07 | 0.11 | 0.07 | 47.9 |
| Appr | ach |  | 58 | 1.8 | 58 | 1.8 | 0.031 | 0.8 | NA | 0.1 | 0.4 | 0.07 | 0.11 | 0.07 | 48.7 |
| North: Margaret St (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 12 | 0.0 | 12 | 0.0 | 0.051 | 4.7 | LOS A | 0.2 | 1.2 | 0.17 | 0.53 | 0.17 | 45.6 |
| 9 | R2 | All MCs | 51 | 0.0 | 51 | 0.0 | 0.051 | 5.0 | LOS A | 0.2 | 1.2 | 0.17 | 0.53 | 0.17 | 43.4 |
| Appr | ach |  | 62 | 0.0 | 62 | 0.0 | 0.051 | 4.9 | LOS A | 0.2 | 1.2 | 0.17 | 0.53 | 0.17 | 43.9 |
| West: Anderson Rd (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | All MCs | 40 | 5.3 | 40 | 5.3 | 0.044 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.26 | 0.00 | 46.1 |
| 11 | T1 | All MCs | 42 | 0.0 | 42 | 0.0 | 0.044 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.26 | 0.00 | 47.9 |
| Approach |  |  | 82 | 2.6 | 82 | 2.6 | 0.044 | 2.2 | NA | 0.0 | 0.0 | 0.00 | 0.26 | 0.00 | 47.0 |
| All Vehicles |  |  | 202 | 1.6 | 202 | 1.6 | 0.051 | 2.7 | NA | 0.2 | 1.2 | 0.07 | 0.30 | 0.07 | 46.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:29 PM
Project: Z:\Jobs\2022l220918\MTE SIDRAI23 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## 目 Site: 5 [(ExAM) Windsor Rd / Anderson Rd (Site Folder: <br> Existing)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Windsor Rd / Anderson Rd
Existing AM Peak
Job No 220918
Site Category: Existing AM
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=277$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Mov Class | $\begin{array}{r} \text { Dem: } \\ \text { Flc } \\ \text { [ Total }+ \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { nand } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{array}{r} \text { rival } \\ \text { lows } \\ \text { HV ] } \\ \% \end{array}$ | Deg. Satn v/c | Aver. Delay $\qquad$ <br> sec | Level of Service | Aver. Q [ Veh. veh | ck Of e Dist ] m | Prop. Que |  | Aver. No. of Cycles | Aver. Speed $\qquad$ km/h |
| South: Windsor Rd (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | All MCs | 1 |  | 1 |  | 0.719 | 12.7 | LOS A | 17.1 | 128.7 | 0.41 | 0.38 | 0.41 | 32.9 |
| 2 | T1 | All MCs | 1127 | 8.9 | 1127 |  | * 0.719 | 7.1 | LOS A | 17.1 | 128.7 | 0.41 | 0.38 | 0.41 | 55.8 |
| 3 | R2 | All MCs | 14 |  | 14 |  | 0.292 | 156.8 | LOS F | 1.2 | 8.2 | 1.00 | 0.70 | 1.00 | 12.2 |
| Appro |  |  | 1142 |  | 1142 |  | 0.719 | 8.9 | LOS A | 17.1 | 128.7 | 0.42 | 0.38 | 0.42 | 53.9 |
| East: Anderson Rd (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | All MCs | 24 |  | 24 |  | 0.103 | 92.2 | LOS F | 1.0 | 6.8 | 0.92 | 0.71 | 0.92 | 22.4 |
| 5 | T1 | All MCs | 4 | 0.0 | 4 |  | * 0.775 | 103.0 | LOS F | 4.4 | 30.7 | 1.00 | 0.83 | 1.09 | 7.5 |
| 6 | R2 | All MCs | 94 |  | 94 |  | 0.775 | 107.6 | LOS F | 4.4 | 30.7 | 1.00 | 0.83 | 1.09 | 16.5 |
| Appro |  |  |  |  |  |  | 0.775 | 104.4 | LOS F | 4.4 | 30.7 | 0.98 | 0.80 | 1.06 | 17.4 |
| North: Windsor Rd (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 22 |  | 22 |  | 0.583 | 10.9 | LOS A | 16.3 | 117.4 | 0.39 | 0.37 | 0.39 | 46.4 |
| 8 | T1 | All MCs | 2678 |  | 2678 |  | 0.583 | 5.3 | LOS A | 16.3 | 117.6 | 0.39 | 0.36 | 0.39 | 54.4 |
| Appro |  |  | 2700 |  | 2700 |  | 0.583 | 5.4 | LOS A | 16.3 | 117.6 | 0.39 | 0.36 | 0.39 | 54.3 |
| West: Club Access (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.074 | 67.6 | LOS E | 0.4 | 3.1 | 0.95 | 0.66 | 0.95 | 15.0 |
| 11 | T1 | All MCs | 6 | 0.0 | 6 | 0.0 | 0.074 | 65.3 | LOS E | 0.4 | 3.1 | 0.95 | 0.66 | 0.95 | 8.7 |
| 12 | R2 | All MCs |  | 100 0 |  | 100 0 | 0.074 | 68.1 | LOS E | 0.4 | 3.1 | 0.95 | 0.66 | 0.95 | 17.9 |
| Approach |  |  |  | 22.2 |  | 22.2 | 0.074 | 66.2 | LOS E | 0.4 | 3.1 | 0.95 | 0.66 | 0.95 | 11.9 |
| All Vehicles |  |  | 3974 |  | 3974 |  | 0.775 | 9.6 | LOS A | 17.1 | 128.7 | 0.42 | 0.38 | 0.42 | 51.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab)
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:30 PM
Project: Z:\Jobs\2022\220918IMTE SIDRAI23 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## 目 Site: 5 [(ExPM) Windsor Rd / Anderson Rd (Site Folder: <br> Existing)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Windsor Rd / Anderson Rd
Existing PM Peak
Job No 220918
Site Category: Existing PM
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=147$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Mov Class |  | $\begin{aligned} & \text { nand } \\ & \text { lows } \\ & \text { HV ] \| } \\ & \% \end{aligned}$ |  | rival ows HV ] \% | Deg. Satn v/c | Aver. Delay $\qquad$ <br> sec | Level of Service | Aver. Q [ Veh. veh | $\begin{aligned} & \text { ck Of } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que |  | Aver. No. of Cycles | Aver. Speed $\qquad$ km/h |
| South: Windsor Rd (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.666 | 8.6 | LOS A | 14.7 | 104.7 | 0.34 | 0.31 | 0.34 | 33.4 |
| 2 | T1 | All MCs | 2220 |  | 2220 |  | 0.666 | 3.5 | LOS A | 14.7 | 104.7 | 0.34 | 0.31 | 0.34 | 56.7 |
| 3 | R2 | All MCs | 23 |  | 23 |  | * 0.146 | 74.6 | LOS F | 1.0 | 7.0 | 0.96 | 0.71 | 0.96 | 20.6 |
| Appro |  |  | 2244 |  | 2244 |  | 0.666 | 4.2 | LOS A | 14.7 | 104.7 | 0.34 | 0.31 | 0.34 | 55.8 |
| East: Anderson Rd (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | All MCs | 8 | 0.0 | 8 |  | 0.023 | 71.8 | LOS F | 0.3 | 2.1 | 0.83 | 0.66 | 0.83 | 24.3 |
| 5 | T1 | All MCs | 6 | 0.0 | 6 | 0.0 | * 0.811 | 97.7 | LOS F | 4.5 | 31.5 | 1.00 | 0.92 | 1.24 | 6.6 |
| 6 | R2 | All MCs | 87 |  | 87 |  | 0.811 | 102.3 | LOS F | 4.5 | 31.5 | 1.00 | 0.92 | 1.24 | 15.5 |
| Appro |  |  | 102 |  |  |  | 0.811 | 99.5 | LOS F | 4.5 | 31.5 | 0.99 | 0.89 | 1.20 | 15.7 |
| North: Windsor Rd (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 56 |  | 56 |  | 0.703 | 16.3 | LOS B | 22.7 | 165.8 | 0.59 | 0.55 | 0.59 | 40.7 |
| 8 | T1 | All MCs | 1907 |  | 1907 |  | * 0.703 | 10.8 | LOS A | 22.7 | 166.3 | 0.59 | 0.55 | 0.59 | 49.6 |
| Approa |  |  | 1963 |  | 1963 | 5.2 | 0.703 | 10.9 | LOS A | 22.7 | 166.3 | 0.59 | 0.55 | 0.59 | 49.4 |
| West: Club Access (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | All MCs | 1 | 0.0 | 1 |  | 0.084 | 2.7 | LOS A | 0.4 | 3.0 | 0.96 | 0.67 | 0.96 | 14.5 |
| 11 | T1 | All MCs | 2 | 0.0 | 2 |  | 0.084 | 75.8 | LOS F | 0.4 | 3.0 | 0.96 | 0.67 | 0.96 | 8.6 |
| 12 | R2 | All MCs |  | 16.7 |  | 16.7 | 0.084 | 78.3 | LOS F | 0.4 | 3.0 | 0.96 | 0.67 | 0.96 | 18.3 |
| Approach |  |  |  | 11.1 | 9 | 11.1 | 0.084 | 69.3 | LOS E | 0.4 | 3.0 | 0.96 | 0.67 | 0.96 | 16.1 |
| All Vehicles |  |  | 4319 | 3.7 | 4319 | 3.7 | 0.811 | 9.7 | LOS A | 22.7 | 166.3 | 0.47 | 0.43 | 0.48 | 50.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)


## SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com

Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:31 PM
Project: Z:\Jobs\2022\220918\MTE SIDRAl23 0718 - KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 1 [(FutAM) Windsor Rd / Mary St (Site Folder: Future)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Windsor Rd / Mary St
Future AM Peak
Job No 220918
Site Category: Future AM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Mov Class |  | and <br> ows <br> HV ] <br> \% | Ar veh/h | rival ows HV ] \% | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \\ \text { Qu } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | ck Of e Dist ] m | Prop. Que |  | Aver. <br> No. of Cycles | Aver. Speed <br> km/h |
| South: Windsor Rd (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $2 \quad \mathrm{~T} 1$ | All MCs | 1252 | 9.2 | 1252 | 9.2 | 0.358 | 0.0 | LOS A | 2.3 | 17.3 | 0.02 | 0.02 | 0.02 | 56.8 |
| 3 R 2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.358 | 3374.9 | LOS F | 2.3 | 17.3 | 0.05 | 0.05 | 0.05 | 47.2 |
| Approach |  | 1253 | 9.2 | 1253 | 9.2 | 0.358 | 2.9 | NA | 2.3 | 17.3 | 0.02 | 0.02 | 0.02 | 56.8 |
| East: Mary St (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | All MCs | 8 | 0.0 | 8 | 0.0 | 1.031 | 232.0 | LOS F | 2.3 | 15.9 | 1.00 | 1.04 | 1.15 | 11.3 |
| 6 R2 | All MCs | 1 | 0.0 | 1 | 0.0 | 1.031 | 83.2 | LOS F | 2.3 | 15.9 | 1.00 | 1.04 | 1.15 | 12.8 |
| Approach |  | 9 | 0.0 | 9 | 0.0 | 1.031 | 215.4 | LOS F | 2.3 | 15.9 | 1.00 | 1.04 | 1.15 | 11.5 |
| North: Windsor Rd (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | All MCs | 15 | 0.0 | 15 | 0.0 | 0.569 | 5.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 57.0 |
| 8 T1 | All MCs | 2151 | 3.7 | 2151 | 3.7 | 0.569 | 0.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.4 |
| Approach |  | 2165 | 3.7 | 2165 | 3.7 | 0.569 | 0.3 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.4 |
| All Vehicles |  | 3428 | 5.7 | 3428 | 5.7 | 1.031 | 1.8 | NA | 2.3 | 17.3 | 0.01 | 0.01 | 0.01 | 57.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:32 PM
Project: Z:\Jobs\2022\220918IMTE SIDRAl23 0718 - KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 1 [(FutPM) Windsor Rd / Mary St (Site Folder: Future)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Windsor Rd / Mary St
Future PM Peak
Job No 220918
Site Category: Future PM
Give-Way (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:33 PM
Project: Z:\Jobs\2022\220918IMTE SIDRAl23 0718 - KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 2 [(FutAM) Mary St / Margaret St (Site Folder: Future)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Mary St / Margaret St
Future AM Peak
Job No 220918
Site Category: Future AM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn Mov ID Class | Dem Fl [ Total veh/h | $\begin{aligned} & \text { nand } \\ & \text { lows } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{array}{r} \text { Arı } \\ \text { Fl } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | rival lows HV ] \% | Deg. Satn $\qquad$ v/c | Aver. Delay $\qquad$ sec | Level of Service | 95\% <br> Q <br> [ Veh. veh | $\begin{gathered} \text { ck Of } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que |  | Aver. No. of Cycles | Aver. Speed $\qquad$ $\mathrm{km} / \mathrm{h}$ |
| South: Margaret St (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 All MCs | 13 | 0.0 | 13 | 0.0 | 0.066 | 4.6 | LOS A | 0.2 | 1.6 | 0.15 | 0.53 | 0.15 | 45.6 |
| 3 R2 All MCs | 68 | 1.5 | 68 | 1.5 | 0.066 | 4.9 | LOS A | 0.2 | 1.6 | 0.15 | 0.53 | 0.15 | 45.4 |
| Approach | 81 | 1.3 | 81 | 1.3 | 0.066 | 4.9 | LOS A | 0.2 | 1.6 | 0.15 | 0.53 | 0.15 | 45.5 |
| East: Mary St (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 All MCs | 85 | 0.0 | 85 | 0.0 | 0.060 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.40 | 0.00 | 46.6 |
| 5 T1 All MCs | 27 | 0.0 | 27 | 0.0 | 0.060 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.40 | 0.00 | 47.7 |
| Approach | 112 | 0.0 | 112 | 0.0 | 0.060 | 3.5 | NA | 0.0 | 0.0 | 0.00 | 0.40 | 0.00 | 46.9 |
| West: Mary St (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 All MCs | 12 | 0.0 | 12 | 0.0 | 0.015 | 0.0 | LOS A | 0.1 | 0.5 | 0.19 | 0.30 | 0.19 | 48.1 |
| 12 R2 All MCs | 13 |  | 13 | 8.3 | 0.015 | 5.2 | LOS A | 0.1 | 0.5 | 0.19 | 0.30 | 0.19 | 46.6 |
| Approach | 25 |  | 25 |  | 0.015 | 2.6 | NA | 0.1 | 0.5 | 0.19 | 0.30 | 0.19 | 47.3 |
| All Vehicles | 219 |  | 219 |  | 0.066 | 3.9 | NA | 0.2 | 1.6 | 0.08 | 0.44 | 0.08 | 46.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:34 PM
Project: Z:\Jobs\2022\220918\MTE SIDRAl23 0718 - KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 2 [(FutPM) Mary St / Margaret St (Site Folder: Future)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Mary St / Margaret St
Future PM Peak
Job No 220918
Site Category: Future PM
Give-Way (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:35 PM
Project: Z:\Jobs\2022\220918\MTE SIDRAl23 0718 - KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 3 [(FutAM) William St / Windermere Ave (Site Folder:

Future)]
Output produced by SIDRA INTERSECTION Version: 9.1.3.210
William St / Windermere Ave
Future AM Peak
Job No 220918
Site Category: Future AM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Mov Class |  | mand lows HV ] [ $\qquad$ |  | rival ows HV ] $\qquad$ | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | ck Of e Dist ] m | Prop. Que | $\begin{aligned} & \text { Eff. } \\ & \text { Stop } \\ & \text { Rate } \end{aligned}$ | Aver. No. of Cycles | Aver. Speed <br> km/h |
| South: Mary St / William St (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | All MCs | 16 | 0.0 | 16 | 0.0 | 0.026 | 4.7 | LOS A | 0.1 | 0.6 | 0.15 | 0.51 | 0.15 | 45.6 |
| 3 | R2 | All MCs | 18 | 0.0 | 18 | 0.0 | 0.026 | 5.1 | LOS A | 0.1 | 0.6 | 0.15 | 0.51 | 0.15 | 45.4 |
| Appr | ach |  | 34 | 0.0 | 34 | 0.0 | 0.026 | 4.9 | LOS A | 0.1 | 0.6 | 0.15 | 0.51 | 0.15 | 45.5 |
| East: Windermere Ave (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | All MCs | 43 | 0.0 | 43 | 0.0 | 0.045 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.27 | 0.00 | 47.3 |
| 5 | T1 | All MCs | 43 | 0.0 | 43 | 0.0 | 0.045 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.27 | 0.00 | 48.5 |
| Approach |  |  | 87 | 0.0 | 87 | 0.0 | 0.045 | 2.3 | NA | 0.0 | 0.0 | 0.00 | 0.27 | 0.00 | 47.9 |
| West: Windermere Ave (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | All MCs | 55 | 5.8 | 55 | 5.8 | 0.054 | 0.0 | LOS A | 0.2 | 1.5 | 0.15 | 0.26 | 0.15 | 48.3 |
| 12 | R2 | All MCs | 41 | 0.0 | 41 | 0.0 | 0.054 | 5.0 | LOS A | 0.2 | 1.5 | 0.15 | 0.26 | 0.15 | 46.9 |
| Appr | ach |  | 96 | 3.3 | 96 | 3.3 | 0.054 | 2.2 | NA | 0.2 | 1.5 | 0.15 | 0.26 | 0.15 | 47.7 |
| All V | icles |  | 216 | 1.5 | 216 | 1.5 | 0.054 | 2.6 | NA | 0.2 | 1.5 | 0.09 | 0.30 | 0.09 | 47.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:35 PM
Project: Z:\Jobs\2022l220918\MTE SIDRAl23 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 3 [(FutPM) William St / Windermere Ave (Site Folder:

Future)]
Output produced by SIDRA INTERSECTION Version: 9.1.3.210
William St / Windermere Ave
Future PM Peak
Job No 220918
Site Category: Future PM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID |  | Mov Class |  | and ows HV ] \% |  | rival ows HV ] \% | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> Q <br> [ Veh. veh | ck Of e Dist ] m | Prop. Que | Eff. <br> Stop <br> Rate | Aver. No. of Cycles | Aver. Speed <br> km/h |
| South: Mary St / William St (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | All MCs | 33 | 0.0 | 33 | 0.0 | 0.033 | 4.7 | LOS A | 0.1 | 0.9 | 0.13 | 0.51 | 0.13 | 45.7 |
| 3 | R2 | All MCs | 14 |  | 14 | 7.6 | 0.033 | 5.2 | LOS A | 0.1 | 0.9 | 0.13 | 0.51 | 0.13 | 45.4 |
| Appr | ach |  | 47 | 2.3 | 47 | 2.3 | 0.033 | 4.8 | LOS A | 0.1 | 0.9 | 0.13 | 0.51 | 0.13 | 45.6 |
| East: Windermere Ave (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | All MCs | 26 | 4.1 | 26 | 4.1 | 0.036 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.21 | 0.00 | 47.6 |
| 5 | T1 | All MCs | 41 | 2.6 | 41 |  | 0.036 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.21 | 0.00 | 48.8 |
| Approach |  |  | 67 | 3.2 | 67 | 3.2 | 0.036 | 1.8 | NA | 0.0 | 0.0 | 0.00 | 0.21 | 0.00 | 48.3 |
| West: Windermere Ave (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | All MCs | 68 | 3.1 | 68 | 3.1 | 0.051 | 0.0 | LOS A | 0.1 | 1.0 | 0.09 | 0.17 | 0.09 | 48.9 |
| 12 | R2 | All MCs | 25 | 0.0 | 25 | 0.0 | 0.051 | 5.0 | LOS A | 0.1 | 1.0 | 0.09 | 0.17 | 0.09 | 47.5 |
| Appr | ach |  | 94 | 2.2 | 94 | 2.2 | 0.051 | 1.3 | NA | 0.1 | 1.0 | 0.09 | 0.17 | 0.09 | 48.5 |
| All V | icles |  | 207 | 2.5 | 207 | 2.5 | 0.051 | 2.3 | NA | 0.1 | 1.0 | 0.07 | 0.26 | 0.07 | 47.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:36 PM
Project: Z:\Jobs\2022l220918\MTE SIDRAl23 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 4 [(FutAM) Anderson Rd / Margaret St (Site Folder:

Future)]
Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Anderson Rd / Margaret St
Future AM Peak
Job No 220918
Site Category: Future AM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Mov Class |  | $\begin{gathered} \text { nand } \\ \text { lows } \\ \text { HV ] [ } \\ \% \end{gathered}$ |  | rival <br> ows <br> HV ] <br> \% | Deg. Satn v/c | Aver. Delay sec | Level of Service |  |  | Prop. Que | $\begin{aligned} & \text { Eff. } \\ & \text { Stop } \\ & \text { Rate } \end{aligned}$ | Aver. No. of Cycles | Aver. Speed <br> km/h |
| East: Anderson Rd (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | All MCs | 76 | 1.4 | 76 | 1.4 | 0.054 | 0.0 | LOS A | 0.1 | 1.0 | 0.09 | 0.15 | 0.09 | 48.5 |
| 6 | R2 | All MCs | 23 | 0.0 | 23 | 0.0 | 0.054 | 5.1 | LOS A | 0.1 | 1.0 | 0.09 | 0.15 | 0.09 | 47.6 |
| Appr |  |  | 99 | 1.1 | 99 | 1.1 | 0.054 | 1.2 | NA | 0.1 | 1.0 | 0.09 | 0.15 | 0.09 | 48.2 |
| North: Margaret St (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 25 | 0.0 | 25 | 0.0 | 0.086 | 4.6 | LOS A | 0.3 | 2.1 | 0.13 | 0.52 | 0.13 | 45.7 |
| 9 | R2 | All MCs | 79 |  | 79 | 1.3 | 0.086 | 5.1 | LOS A | 0.3 | 2.1 | 0.13 | 0.52 | 0.13 | 43.5 |
| Appr |  |  | 104 | 1.0 | 104 | 1.0 | 0.086 | 5.0 | LOS A | 0.3 | 2.1 | 0.13 | 0.52 | 0.13 | 44.2 |
| West: Anderson Rd (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | All MCs | 65 | 1.6 | 65 | 1.6 | 0.044 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.42 | 0.00 | 44.9 |
| 11 | T1 | All MCs | 17 | 0.0 | 17 | 0.0 | 0.044 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.42 | 0.00 | 46.5 |
| Approach |  |  | 82 | 1.3 | 82 | 1.3 | 0.044 | 3.6 | NA | 0.0 | 0.0 | 0.00 | 0.42 | 0.00 | 45.2 |
| All Vehicles |  |  | 285 | 1.1 | 285 | 1.1 | 0.086 | 3.3 | NA | 0.3 | 2.1 | 0.08 | 0.37 | 0.08 | 45.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:37 PM
Project: Z:\Jobs\2022l220918\MTE SIDRAl23 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## $\nabla$ Site: 4 [(FutPM) Anderson Rd / Margaret St (Site Folder: Future)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Anderson Rd / Margaret St
Future PM Peak
Job No 220918
Site Category: Future PM
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Mov Class |  | and <br> ows <br> HV ] <br> \% |  | rival ows HV ] $\qquad$ | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | ck Of e Dist ] m | Prop. Que | $\begin{aligned} & \text { Eff. } \\ & \text { Stop } \\ & \text { Rate } \end{aligned}$ | Aver. No. of Cycles | Aver. Speed |
| East: Anderson Rd (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | All MCs | 48 | 2.2 | 48 | 2.2 | 0.035 | 0.0 | LOS A | 0.1 | 0.7 | 0.10 | 0.16 | 0.10 | 48.4 |
| 6 | R2 | All MCs | 16 | 0.0 | 16 | 0.0 | 0.035 | 5.1 | LOS A | 0.1 | 0.7 | 0.10 | 0.16 | 0.10 | 47.5 |
| Appr | ach |  | 65 | 1.6 | 65 | 1.6 | 0.035 | 1.3 | NA | 0.1 | 0.7 | 0.10 | 0.16 | 0.10 | 48.1 |
| North: Margaret St ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 18 | 0.0 | 18 | 0.0 | 0.072 | 4.7 | LOS A | 0.2 | 1.7 | 0.18 | 0.53 | 0.18 | 45.6 |
| 9 | R2 | All MCs | 70 | 0.0 | 70 | 0.0 | 0.072 | 5.0 | LOS A | 0.2 | 1.7 | 0.18 | 0.53 | 0.18 | 43.4 |
| Approach |  |  | 88 | 0.0 | 88 | 0.0 | 0.072 | 5.0 | LOS A | 0.2 | 1.7 | 0.18 | 0.53 | 0.18 | 44.0 |
| West: Anderson Rd (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | All MCs | 50 | 4.2 | 50 | 4.2 | 0.049 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.29 | 0.00 | 45.8 |
| 11 | T1 | All MCs | 42 | 0.0 | 42 | 0.0 | 0.049 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.29 | 0.00 | 47.6 |
| Approach |  |  | 92 | 2.3 |  | 2.3 | 0.049 | 2.5 | NA | 0.0 | 0.0 | 0.00 | 0.29 | 0.00 | 46.6 |
| All Vehicles |  |  | 245 |  | 245 |  | 0.072 | 3.1 | NA | 0.2 | 1.7 | 0.09 | 0.34 | 0.09 | 46.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:38 PM
Project: Z:\Jobs\2022l220918\MTE SIDRAI23 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## Site: 5 [(FutAM) Windsor Rd / Anderson Rd (Site Folder: <br> Future)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Windsor Rd / Anderson Rd
Future AM Peak
Job No 220918
Site Category: Future AM
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=271$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Mov Class |  | and <br> ows <br> HV ] |  | $\begin{aligned} & \text { Arrival } \\ & \text { Flows } \\ & \text { I HV ] } \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | Aver. [ Q veh. veh |  | Prop. Que | $\begin{aligned} & \text { Eff. } \\ & \text { Stop } \\ & \text { Rate } \end{aligned}$ | Aver. No. of Cycles | Aver. Speed km/h |
| South: Windsor Rd (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.752 | 17.3 | LOS B | 21.6 | 163.0 | 0.51 | 0.47 | 0.51 | 31.8 |
| 2 | T1 | All MCs | 1127 | 8.9 | 1127 | 8.9 | * 0.752 | 11.7 | LOS A | 21.6 | 163.0 | 0.51 | 0.47 | 0.51 | 53.9 |
| 3 | R2 | All MCs | 25 | 0.0 | 25 | 0.0 | * 0.522 | 157.1 | LOS F | 2.1 | 14.8 | 1.00 | 0.73 | 1.00 | 12.3 |
| Appr | ach |  | 1153 | 8.7 | 1153 | 8.7 | 0.752 | 14.9 | LOS B | 21.6 | 163.0 | 0.52 | 0.47 | 0.52 | 50.9 |
| East: Anderson Rd (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | All MCs | 36 | 0.0 | 36 | 0.0 | 0.140 | 96.6 | LOS F | 1.3 | 9.3 | 0.92 | 0.72 | 0.92 | 22.9 |
| 5 | T1 | All MCs | 4 | 0.0 | 4 | 0.0 | * 0.812 | 109.5 | LOS F | 5.0 | 35.3 | 1.00 | 0.85 | 1.12 | 7.5 |
| 6 | R2 | All MCs | 105 |  | 105 | 1.0 | 0.812 | 114.1 | LOS F | 5.0 | 35.3 | 1.00 | 0.85 | 1.12 | 16.5 |
| Appr | ach |  | 145 |  |  | 0.7 | 0.812 | 109.7 | LOS F | 5.0 | 35.3 | 0.98 | 0.82 | 1.07 | 17.8 |
| North: Windsor Rd (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 22 | 0.0 | 22 | 0.0 | 0.608 | 12.8 | LOS A | 18.8 | 135.5 | 0.46 | 0.43 | 0.46 | 44.3 |
| 8 | T1 | All MCs | 2678 | 3.3 | 2678 | 3.3 | * 0.608 | 7.2 | LOS A | 18.9 | 135.7 | 0.46 | 0.43 | 0.46 | 52.6 |
| Approach |  |  | 2700 | 3.2 | 2700 | 3.2 | 0.608 | 7.3 | LOS A | 18.9 | 135.7 | 0.46 | 0.43 | 0.46 | 52.6 |
| West: Club Access (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | All MCs | 1 | 0.0 |  | 0.0 | 0.067 | 64.7 | LOS E | 0.4 | 3.1 | 0.94 | 0.65 | 0.94 | 15.4 |
| 11 | T1 | All MCs | 60.0 |  |  | 0.0 | 0.067 | 62.4 | LOS E | 0.4 | 3.1 | 0.94 | 0.65 | 0.94 | 9.0 |
|  | R2 | All MCs | 2100. |  | $\begin{array}{r} 2100 \\ 0 \\ \hline \end{array}$ |  | 0.067 | 65.6 | LOS E | 0.4 | 3.1 | 0.94 | 0.65 | 0.94 | 18.4 |
| Appr | ach |  | 922.2 |  | 922.2 |  | 0.067 | 63.3 | LOS E | 0.4 | 3.1 | 0.94 | 0.65 | 0.94 | 12.3 |
| All Ve | hicles |  | 40084.840084 .8 |  |  |  | 0.812 | 13.3 | LOS A | 21.6 | 163.0 | 0.50 | 0.46 | 0.50 | 49.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)


## SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com

Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:39 PM
Project: Z:IJobsL2022l220918IMTE SIDRA123 07 18-KL - LS Edits.sip9

## MOVEMENT SUMMARY

## 目 Site: 5 [(FutPM) Windsor Rd / Anderson Rd (Site Folder: <br> Future)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210
Windsor Rd / Anderson Rd
Future PM Peak
Job No 220918
Site Category: Future PM
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=147$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Mov Class | Dem Flo [ Total veh/h | mand <br> ows <br> HV ] <br> \% |  | rival lows HV ] \% | Deg. Satn v/c | Aver. <br> Delay <br> sec | Level of Service | Aver. $\qquad$ <br> [ Veh. veh | ck Of le Dist ] m | Prop. Que |  | Aver. No. of Cycles | Aver. Speed km/h |
| South: Windsor Rd (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | All MCs | 1 |  | 1 | 0.0 | 0.667 | 8.6 | LOS A | 14.7 | 105.0 | 0.34 | 0.31 | 0.34 | 33.4 |
| 2 | T1 | All MCs | 2220 | 2.4 | 2220 |  | 0.667 | 3.5 | LOS A | 14.7 | 105.0 | 0.34 | 0.31 | 0.34 | 56.6 |
| 3 | R2 | All MCs | 33 |  | 33 |  | * 0.207 | 75.1 | LOS F | 1.4 | 10.0 | 0.96 | 0.73 | 0.96 | 20.5 |
| Appro |  |  | 2254 | 2.4 | 2254 |  | 0.667 | 4.5 | LOS A | 14.7 | 105.0 | 0.35 | 0.31 | 0.35 | 55.5 |
| East: Anderson Rd (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | All MCs | 18 |  | 18 |  | 0.050 | 77.5 | LOS F | 0.6 | 4.5 | 0.84 | 0.69 | 0.84 | 24.1 |
| 5 | T1 | All MCs | 6 | 0.0 | 6 | 0.0 | * 0.924 | 113.5 | LOS F | 5.3 | 37.4 | 1.00 | 1.03 | 1.45 | 6.2 |
| 6 | R2 | All MCs | 97 |  |  |  | 0.924 | 118.1 | LOS F | 5.3 | 37.4 | 1.00 | 1.03 | 1.45 | 14.3 |
| Appro |  |  | 122 |  | 122 |  | 0.924 | 111.8 | LOS F | 5.3 | 37.4 | 0.98 | 0.98 | 1.36 | 15.1 |
| North: Windsor Rd (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 56 |  | 56 |  | 0.703 | 16.3 | LOS B | 22.7 | 165.8 | 0.59 | 0.55 | 0.59 | 40.7 |
| 8 | T1 | All MCs | 1907 |  | 1907 |  | * 0.703 | 10.8 | LOS A | 22.7 | 166.3 | 0.59 | 0.55 | 0.59 | 49.6 |
| Appro |  |  | 1963 | 5.2 | 1963 |  | 0.703 | 10.9 | LOS A | 22.7 | 166.3 | 0.59 | 0.55 | 0.59 | 49.4 |
| West: Club Access (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.084 | 2.5 | LOS A | 0.4 | 3.0 | 0.96 | 0.67 | 0.96 | 14.5 |
| 11 | T1 | All MCs | 2 | 0.0 | 2 | 0.0 | 0.084 | 75.8 | LOS F | 0.4 | 3.0 | 0.96 | 0.67 | 0.96 | 8.3 |
| 12 | R2 | All MCs |  | 16.7 |  | 16.7 | 0.084 | 78.2 | LOS F | 0.4 | 3.0 | 0.96 | 0.67 | 0.96 | 18.2 |
| Approach |  |  |  | 11.1 | 9 | 11.1 | 0.084 | 69.2 | LOS E | 0.4 | 3.0 | 0.96 | 0.67 | 0.96 | 16.0 |
| All Vehicles |  |  | 4349 | 3.7 | 4349 | 3.7 | 0.924 | 10.6 | LOS A | 22.7 | 166.3 | 0.48 | 0.44 | 0.49 | 50.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Options tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.
Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

* Critical Movement (Signal Timing)


## SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com

Organisation: MCLAREN TRAFFIC ENGINEERING | Licence: NETWORK / 1PC | Processed: Tuesday, 1 August 2023 2:38:40 PM
Project: Z:\Jobs\2022\220918\MTE SIDRAl23 0718 - KL - LS Edits.sip9


ANNEXURE D: TCS PLANS
(1 SHEET)






ANNEXURE F: QUEUING ANALYSIS
(1 SHEET)

## Multi-Server Queue Worksheet

| Service Bays | 24 | Arrival Rate <br> (vehicles/hour) | 32 | Wait Time in Each Bay (seconds) | 496 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Vehicles/Second IN | 0.008888889 | Vehicles/Second <br> OUT (per bay) | 0.002016129 |  |  |
| P0 | 0.012168692 | rho | 4.408888889 | rho (single bay system assumed) | 0.1837 |


| n | 1st Term | Pn | $P(>=n)$ |
| :---: | :---: | :---: | :---: |
| 0 | 1 | 1.22\% | 98.78\% |
| 1 | 4.40889 | 5.37\% | 93.42\% |
| 2 | 9.71915 | 11.83\% | 81.59\% |
| 3 | 14.2836 | 17.38\% | 64.21\% |
| 4 | 15.7436 | 19.16\% | 45.05\% |
| 5 | 13.8824 | 16.89\% | 28.16\% |
| 6 | 10.201 | 12.41\% | 15.75\% |
| 7 | 6.42501 | 7.82\% | 7.93\% |
| 8 | 3.54089 | 4.31\% | 3.62\% |
| 9 | 1.7346 | 2.11\% | 1.51\% |
| 10 | 0.76477 | 0.93\% | 0.58\% |
| 11 | 0.30652 | 0.37\% | 0.20\% |
| 12 | 0.11262 | 0.14\% | 0.07\% |
| 13 | 0.03819 | 0.05\% | 0.02\% |
| 14 | 0.01203 | 0.01\% | 0.01\% |

$\left.\begin{array}{|c|c|}\hline \text { Percentile } & \text { Number of Vehicles in System }\end{array} \begin{array}{c}\text { Number } \\ \text { of } \\ \text { Vehicles } \\ \text { Queued }\end{array}\right\}$


ANNEXURE G: SWEPT PATH TESTING (5 SHEETS)


AUSTRALIAN STANDARD $85^{\text {TH }}$ PERCENTILE SIZE VEHICLE (B85)


AUSTRALIAN STANDARD 99.8 ${ }^{\text {TH }}$ PERCENTILE SIZE VEHICLE (B99)
Blue - Tyre Path
Green - Vehicle Body
Red - 300mm Clearance
Tested @ 5-km/h internally; 10-km/h on public roads.


B85 / B99 TWO-WAY PASSING AT THE VEHICLE CROSSOVER Successful


B85 / B99 TWO-WAY PASSING ALONG BASEMENT RAMP Successful


B85 ENTRY / EXIT FROM SPACE 13
Successful - 2 manoeuvres REVERSE IN / 1 manoeuvre FORWARD OUT


B85 ENTRY / EXIT FROM SPACE 8
Successful - 2 manoeuvres REVERSE IN / 1 manoeuvre FORWARD OUT

